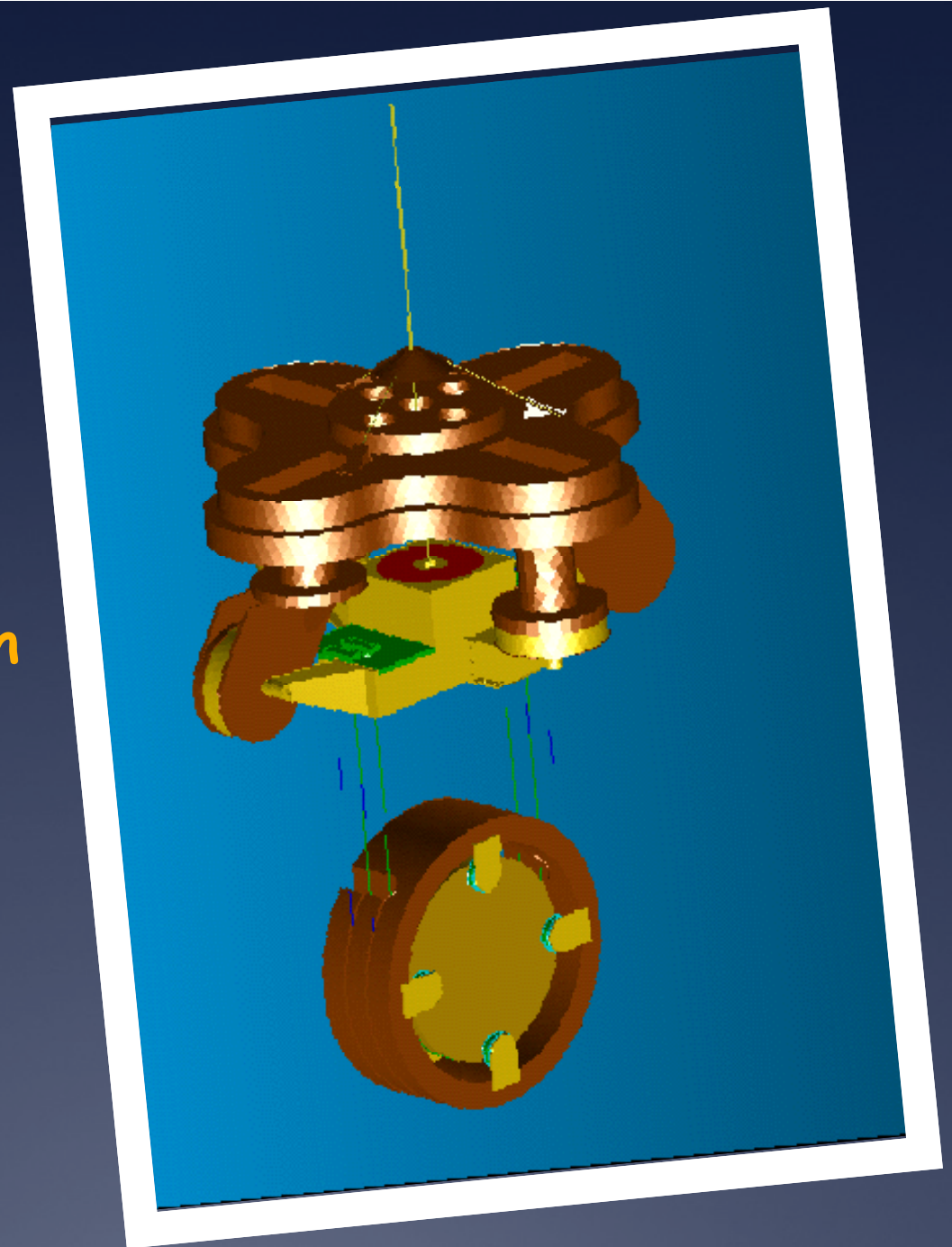


# A Full Scale Cryogenic Payload for 3<sup>rd</sup> generation GW Interferometers

PAOLA PUPPO  
*INFN-ROME*



# Why to cool the mirrors?

- ⌘ Test masses and suspensions thermal noise reduces at low temperature:

$$\langle x^2 \rangle \propto T$$

- ⌘ Thermoelastic noise both of the mirror substrates and coatings decrease:

$$\langle x^2 \rangle \propto \alpha T^2$$

Thermal expansion rate  $\alpha$  decreases at low temperature;

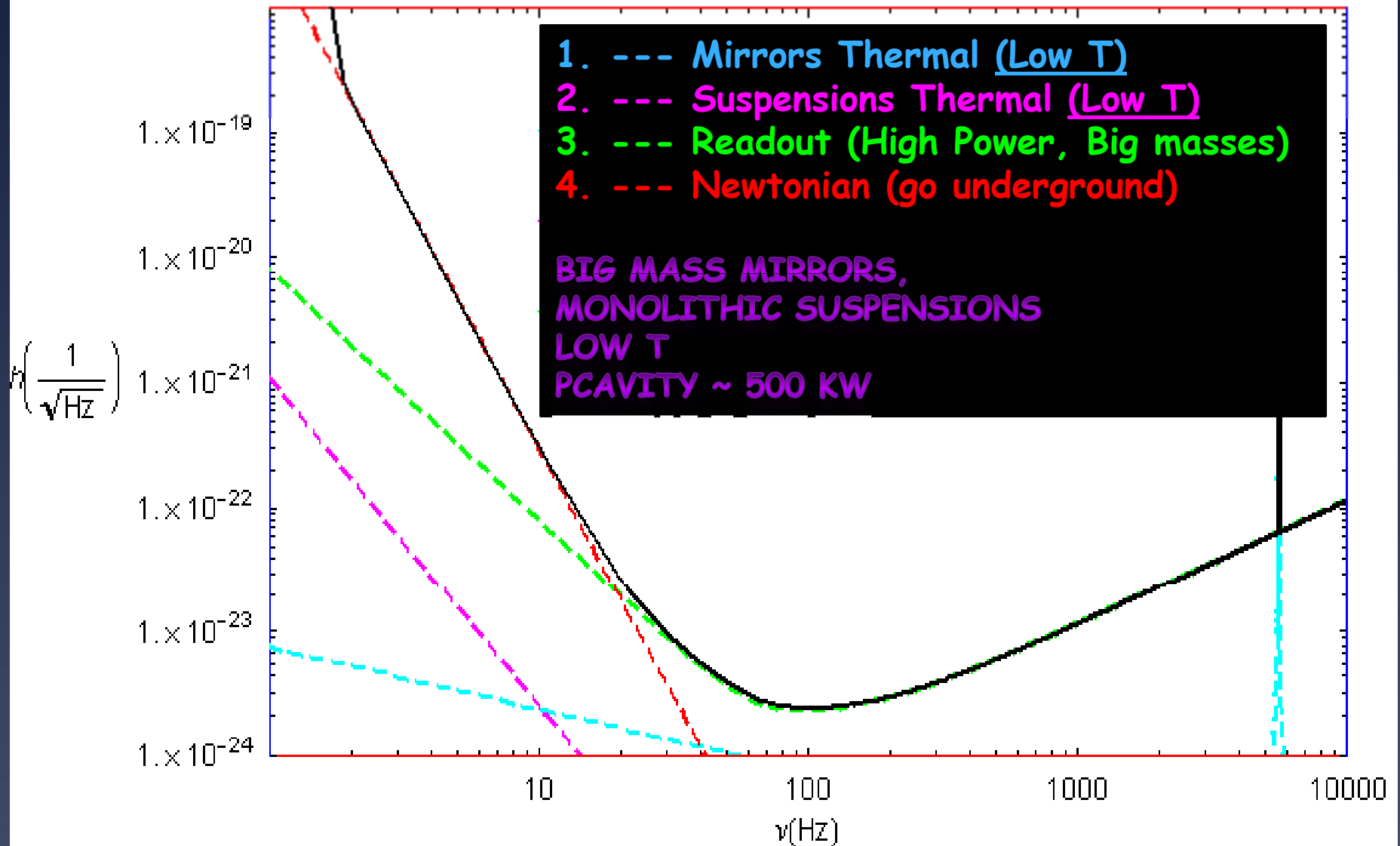
- ⌘ Thermorefractive noise

$$\langle x^2 \rangle \propto T^2$$

- ⌘ Losses of some materials decrease at low temperature

$$\langle x^2 \rangle \propto T \Phi$$

# Cryogenic 3<sup>o</sup> Generation GW detector



... to prepare for the future:

- Mirror cooling techniques

- Payload structure

- Cryogenic interface with low frequency suspensions

- Sensors and Actuators using superconducting/cryogenic techniques:

  - dcSQUIDs amplifiers,

  - Superconducting pancake coils (inductive sensors)

  - Electrostatic Cryogenic Sensors

- Superconducting e.m. shielding

# CRYO-COMPATIBLE MIRROR SUSPENSION DESIGN

•High Thermal impedance MRM wire

(The upper part is thermally insulated by thermal screens)

Superconducting e.m. shielding

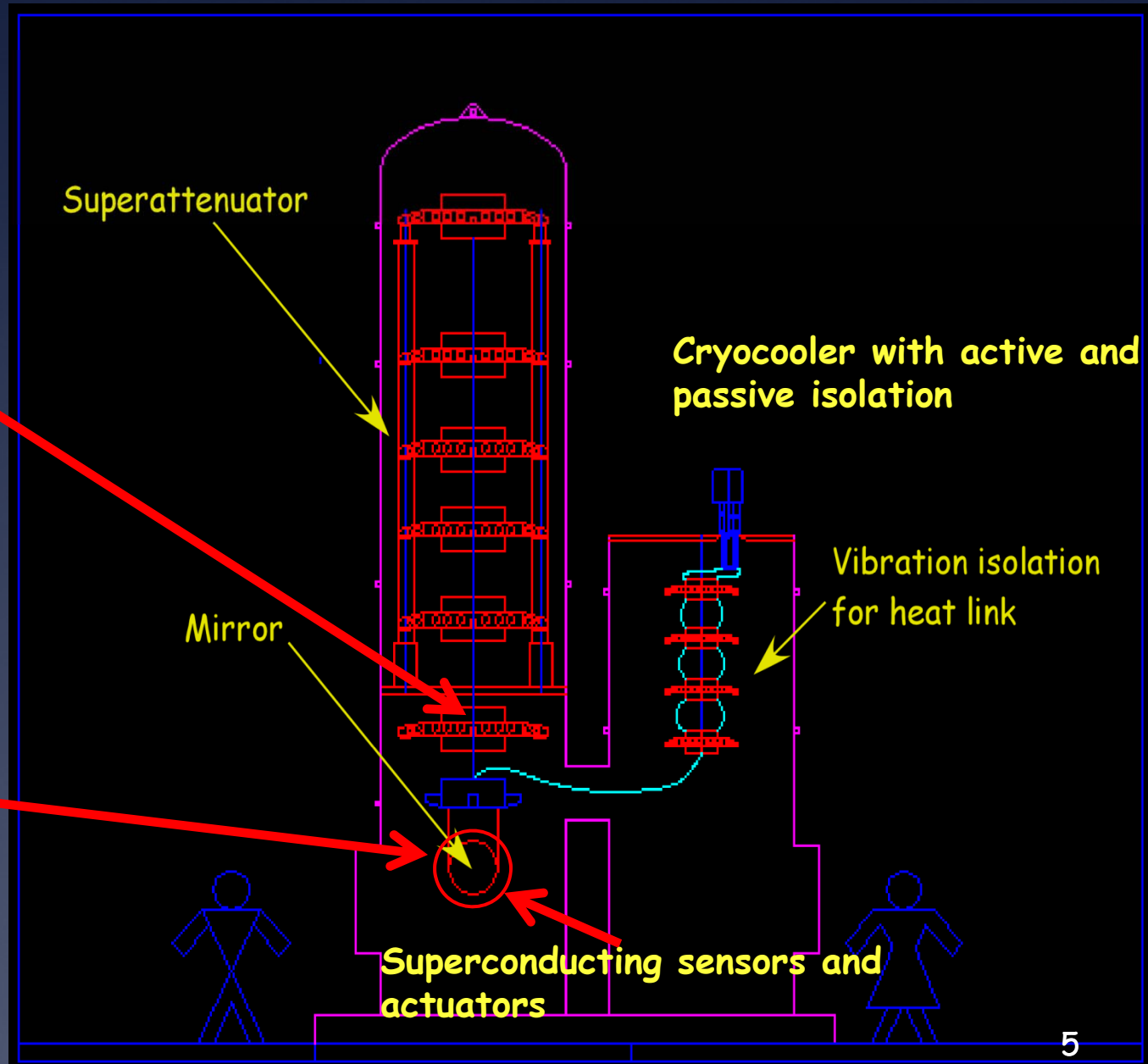
Superattenuator

Cryocooler with active and passive isolation

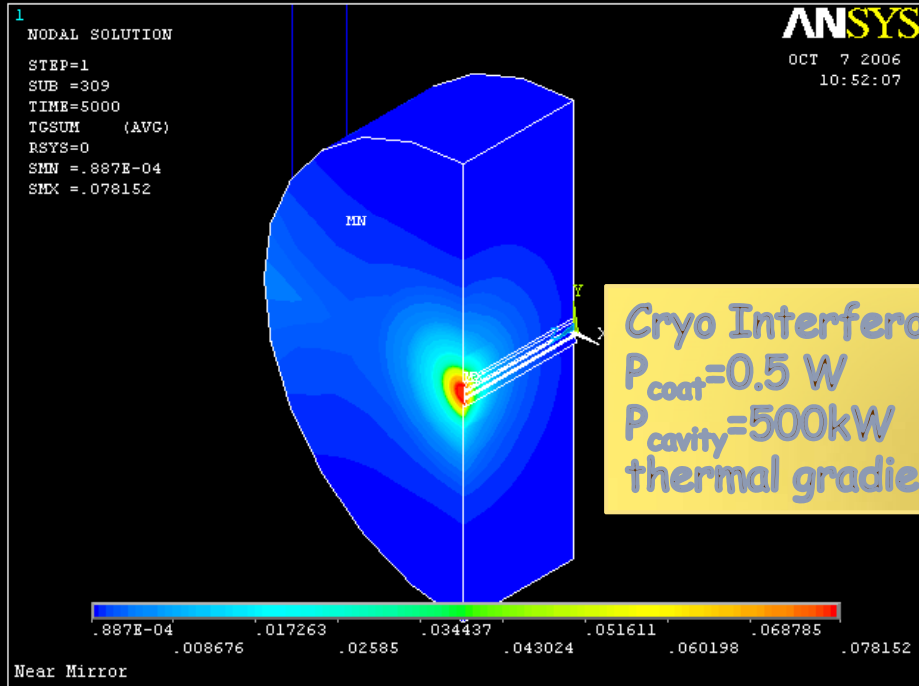
Vibration isolation for heat link

Mirror

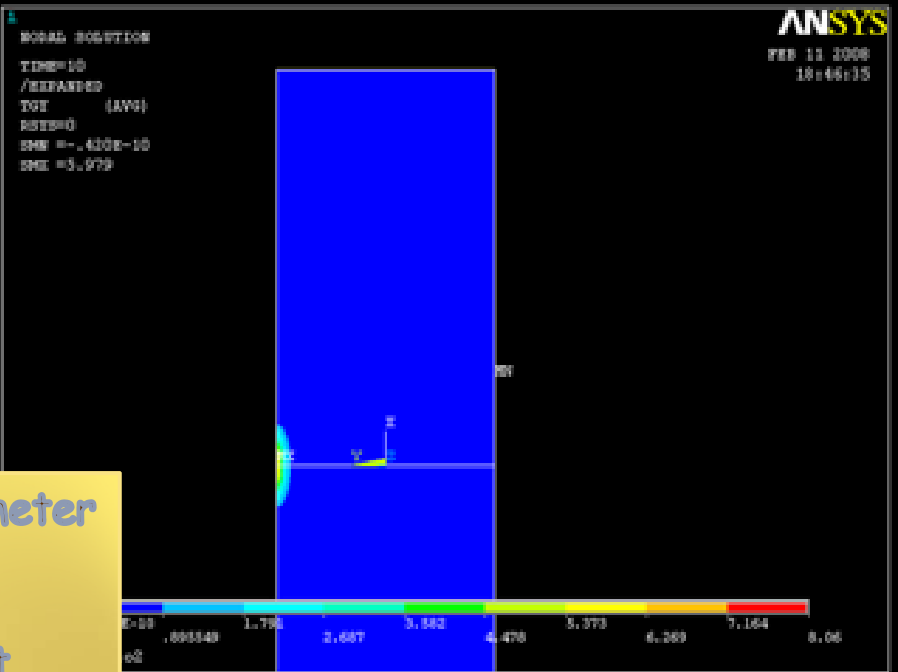
Superconducting sensors and actuators



# Crucial motivation for cryogenic application: mirror thermal lensing



Cryo Interferometer  
 $P_{coat} = 0.5 \text{ W}$   
 $P_{cavity} = 500 \text{ kW}$   
 thermal gradient





# How can we cool the mirrors?

## ➤ Mirror and its suspension wires:

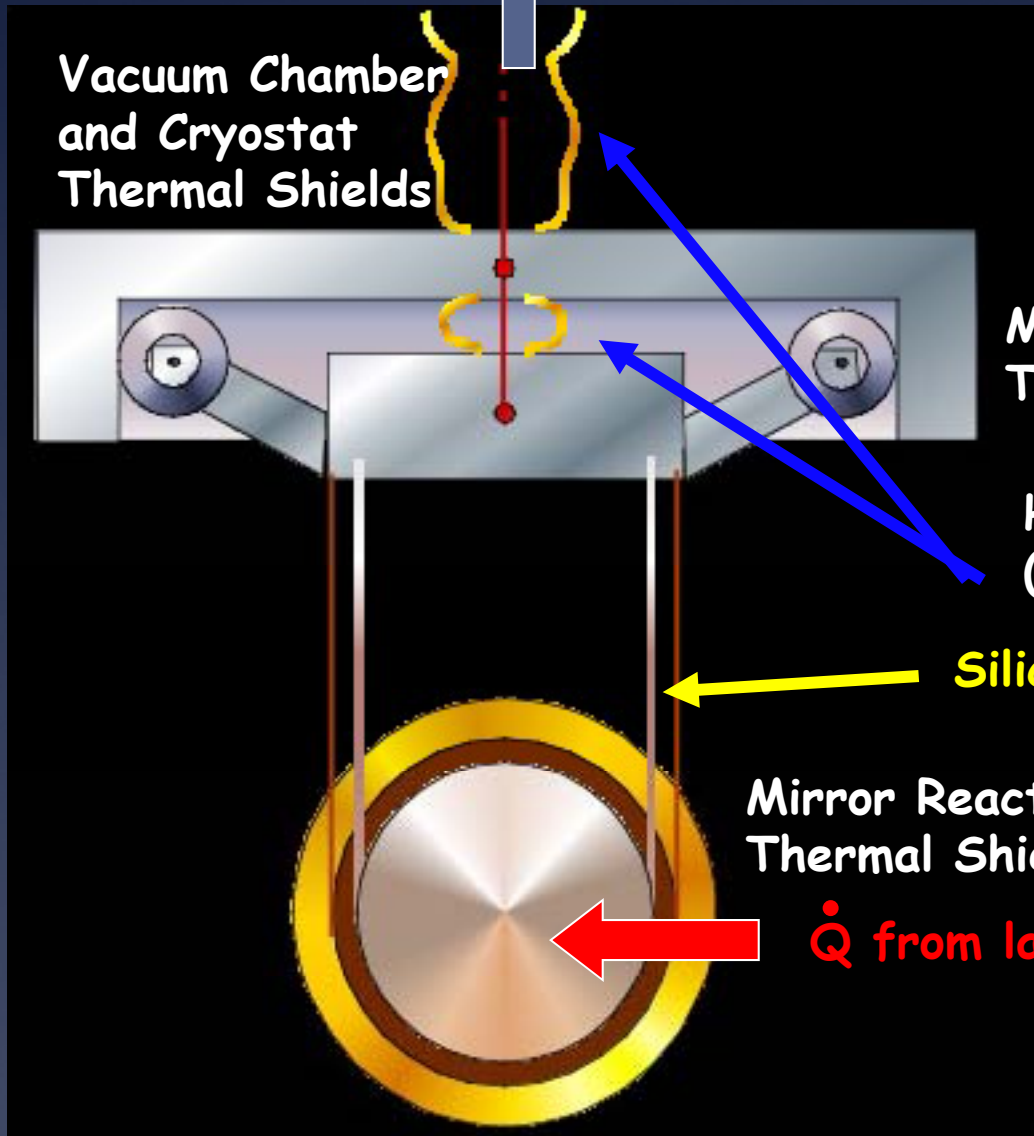
- wires and mirror materials compatible with good mechanical and thermal properties;
  - High thermal conductivities materials;
  - Low mechanical and optical losses;

a promising material both as mirror substrate and wire is silicon having

- high thermal conductivity
- very low thermal expansion (zero below 17K)

# Principle scheme

$\dot{Q}$  from refrigerator



Marionetta Reaction Mass:  
Thermal Shield

High Efficiency Soft Thermal Links  
(e.g. pure Al, copper)

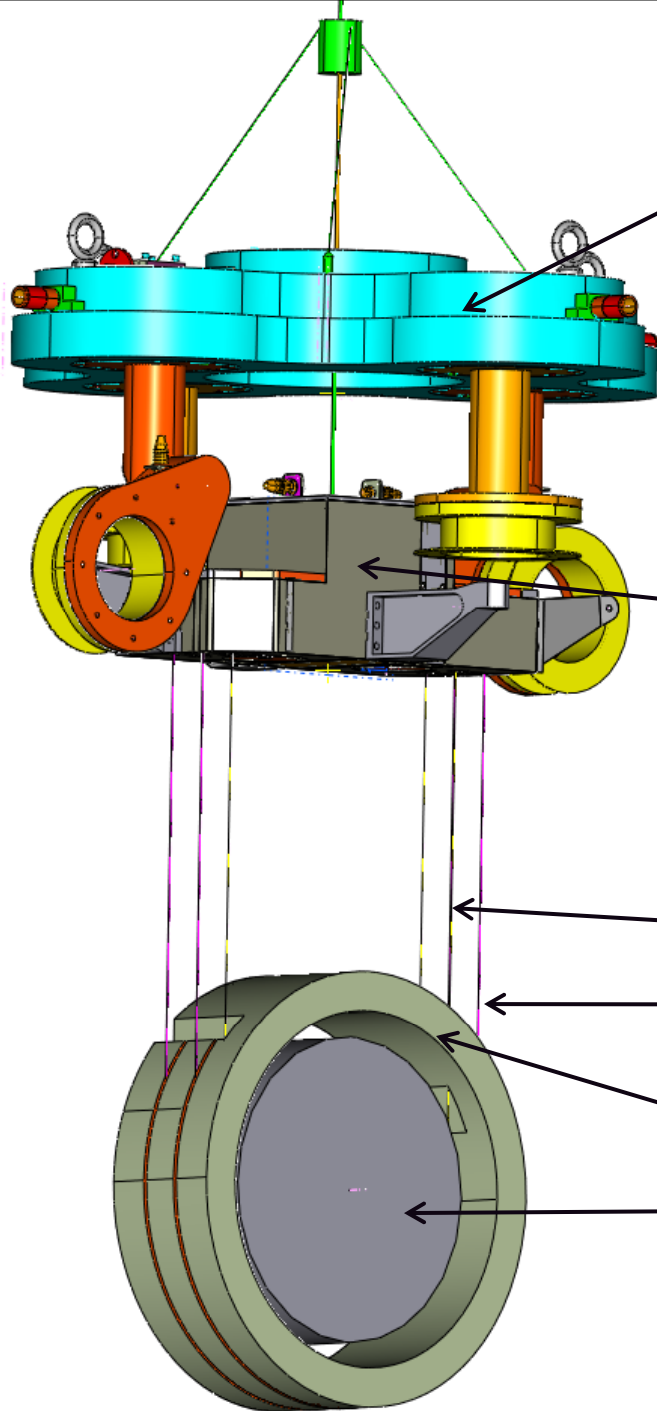
Silicon Monolithic Suspension

Mirror Reaction Mass:  
Thermal Shield

$\dot{Q}$  from laser beam



## 2008: Full Scale Cryogenic Payload



•Marionetta Reaction Mass (MRM)

•Ti alloy cable (low thermal conductivity) Ti-6Al-4V

•Marionetta

•Mirror silicon Wires

•Reaction Mass high conductive wires

•Reaction Mass (Al Alloy)

•Silicon mirror

### Main Requirements

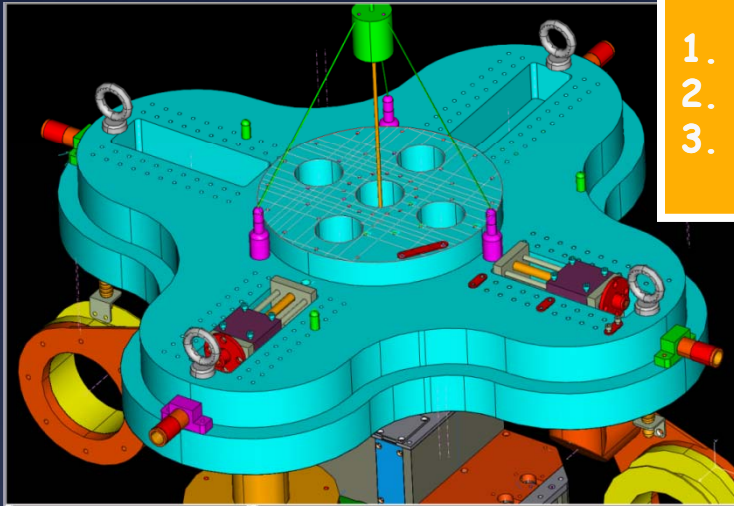
1. Internal frequencies as high as possible
2. Low pendulum and torsional frequencies (mirror control).
3. Good thermal properties for cryogenic operation



# Reaction Masses

## Mirror's

### Marionetta's

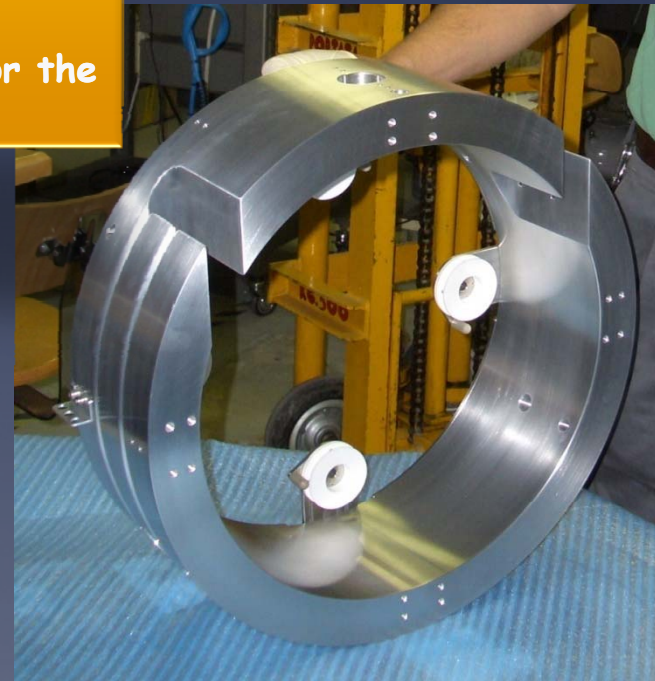
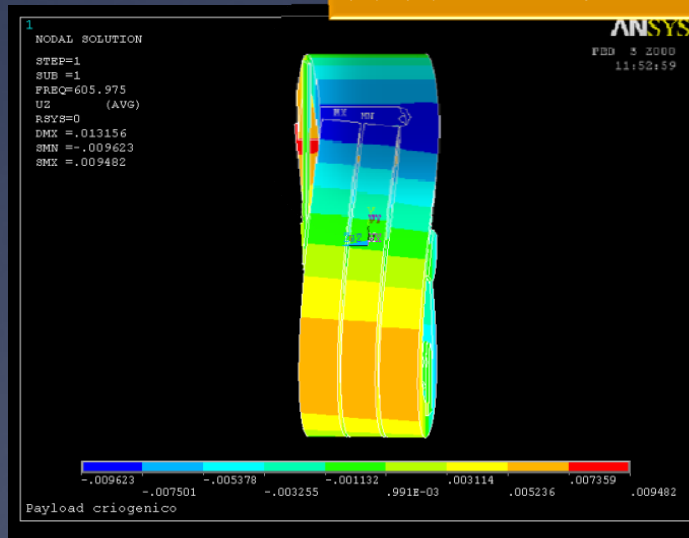
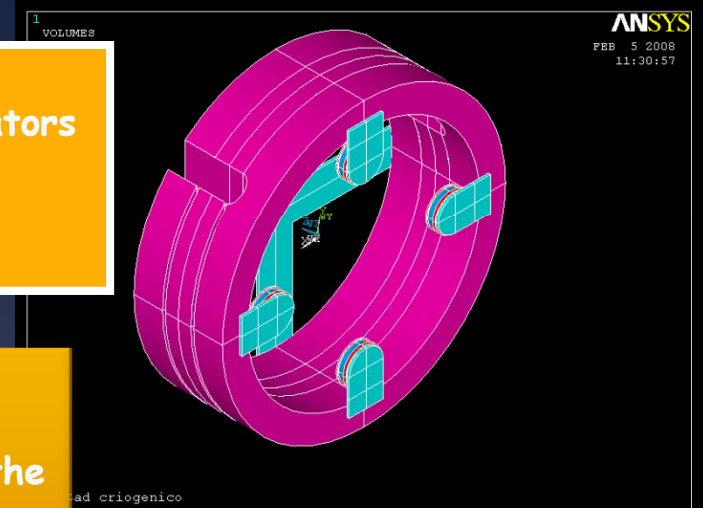


- Main Properties**
1. Supports the e.m. actuators
  2. Act as thermal screen
  3. Protect the mirror
- Made of Al alloy

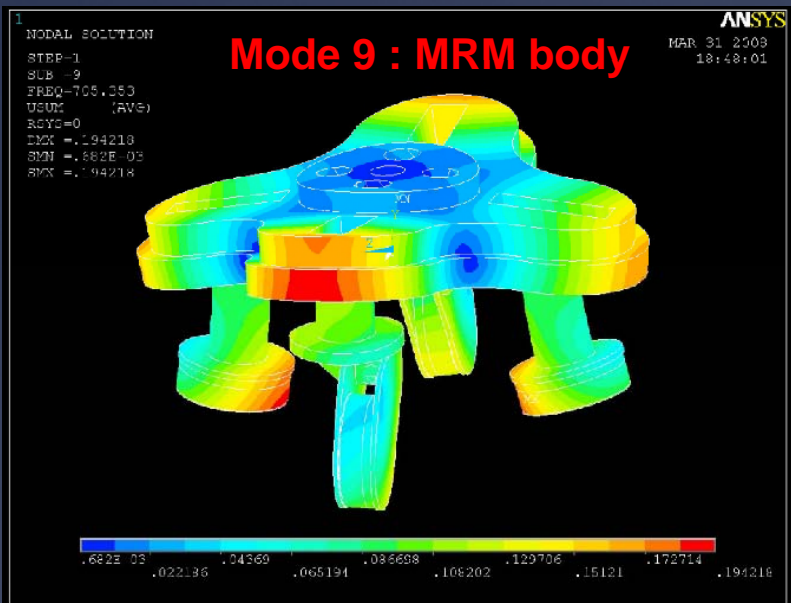
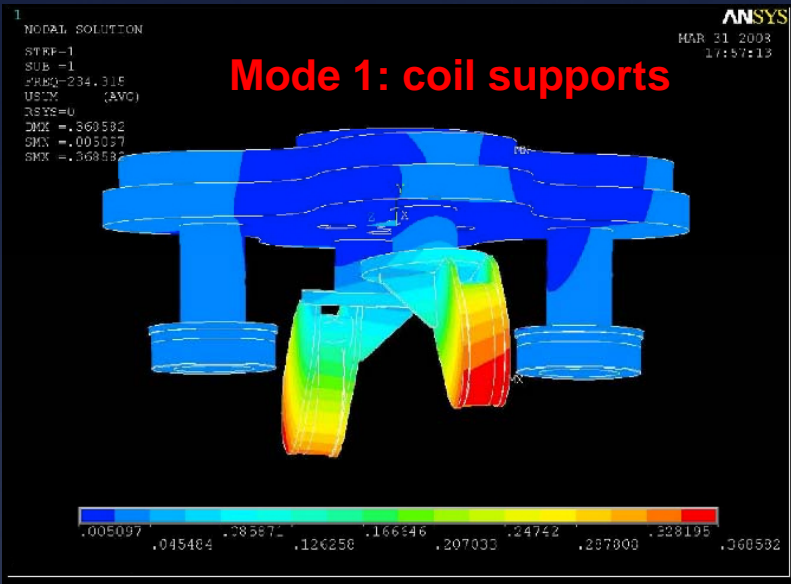
### FEM mechanical

Lowest frequency for the Mirror RM: 600 Hz

Lowest frequency for the MRM: 400 Hz

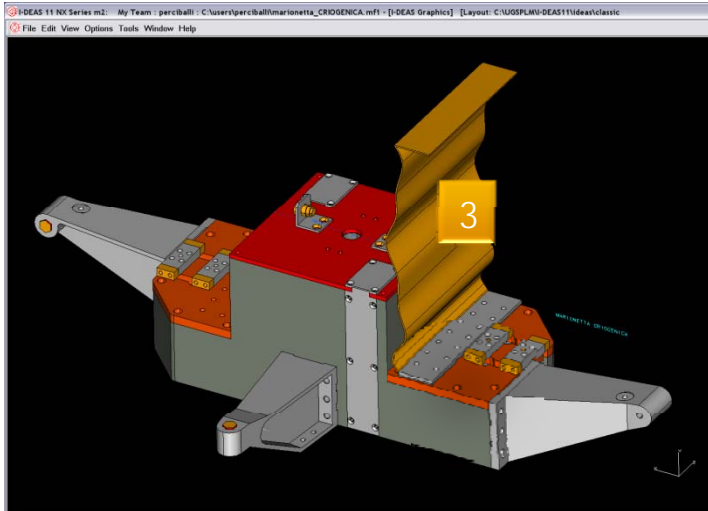


# FEM study of the MRM



Mode number	Frequency (Hz)	Mode identification
1	234	Bending of the horizontal coil support
2	262	Bending of the horizontal coil support
3	270	Bending of the horizontal coil support
4	300	Bending of the horizontal coil support
5	377	Bending of the vertical coil support
6	419	Bending of the vertical coil support
7	472	Bending of the vertical coil support
8	476	Bending of the vertical coil support
9	705	Anti symmetric butterfly mode of the plate
10	755	2 <sup>o</sup> harm. of the Bending of the horiz. coil support
11	763	2 <sup>o</sup> harm. of the Bending of the horiz. coil support
12	789	Longitudinal vibration of the vertical coil support
13	794	Longitudinal vibration of the vertical coil support
14	1106	Longitudinal vibration of the horizontal coil support
15	1164	Torsion mode of the plate
16	1171	Torsion mode of the plate
17	1316	Radial mode of the plate
18	1382	Symmetric butterfly mode of the plate
19	1544	Radial mode of the plate
20	1621	Torsion mode of the plate

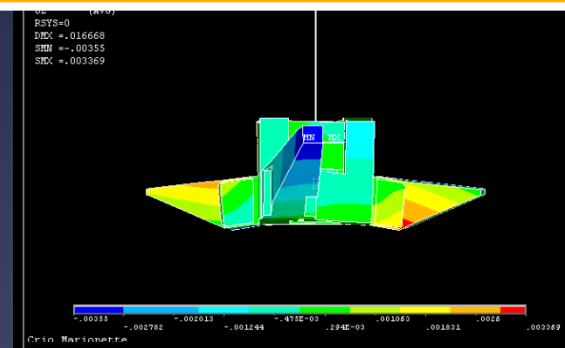
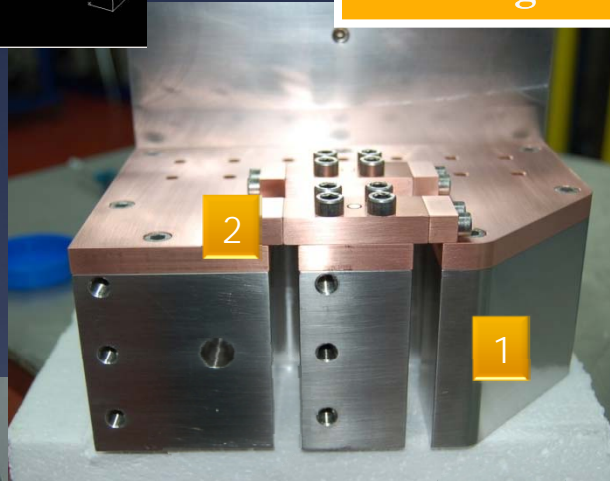




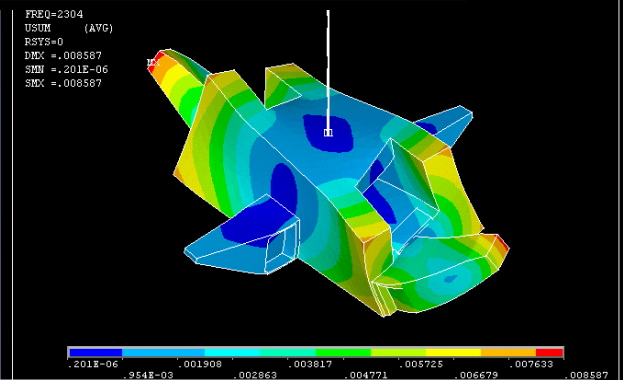
# Marionetta

## Main Characteristics

1. Lateral cuts for the insertion of the silicon wires
2. Copper clamps
3. Copper links with the cooler
4. Dielectric arms epoglass FR4 (no eddy currents)
5. No magnetic steel body



ANSYS  
MAY 13 2008  
13:55:33



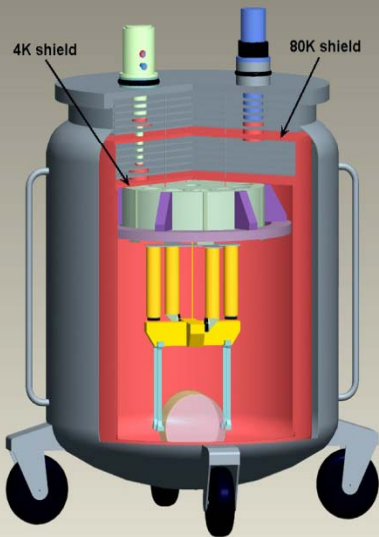
## Marionetta internal modes

Body: lowest 2300 kHz  
Arms: lowest 1100 Hz

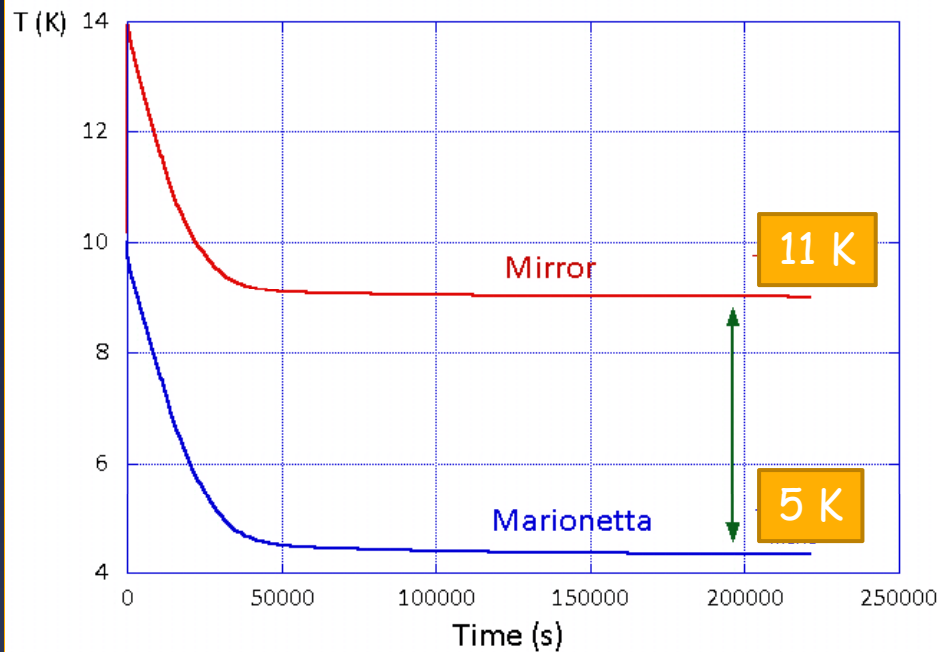
# The Cryogenic Test Facility

F. Frasconi, R. Passaquieti (Pisa) A. Pasqualetti, (EGO)

- \* Cryostat built in Cascina (Virgo site - 1500 West Arm)
- \* Equipped with 2 pulse tube cryogenerators (1 double-stage (0.5W @ 4.5 K), 1 single stage PT60)

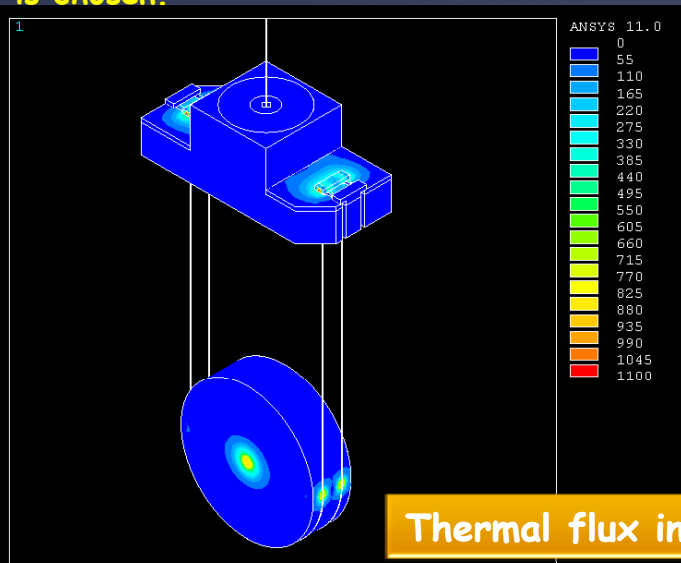
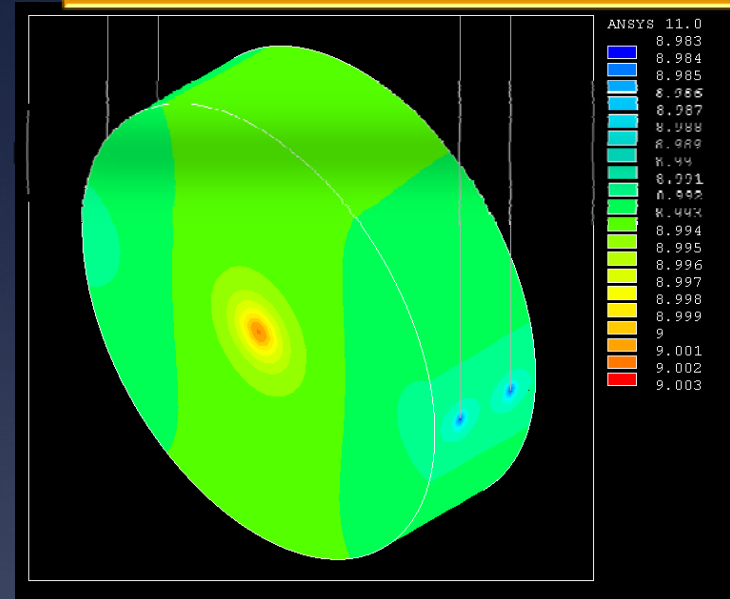


# The transient FEM thermal simulation



•To optimize the cooling time a wire diameter of 3.0mm is chosen.

## Steady state Mirror temperature



Thermal flux in the steady state

$$P_{cooler}(T_{mario}) = P_{abs} = 1 \text{ W} \Rightarrow T_{mario} = 5 \text{ K}$$

$$P_{abs} = 4 \frac{\Sigma_w}{L} K_{mean} (T_{mario} - T_{mirror})$$

$$K_{mean} = \frac{1}{\Delta T} \int_{T_{mario}}^{T_{mirror}} K_{copper}(T) dT \cong 16000 \frac{\text{W}}{\text{m} \cdot \text{K}}$$

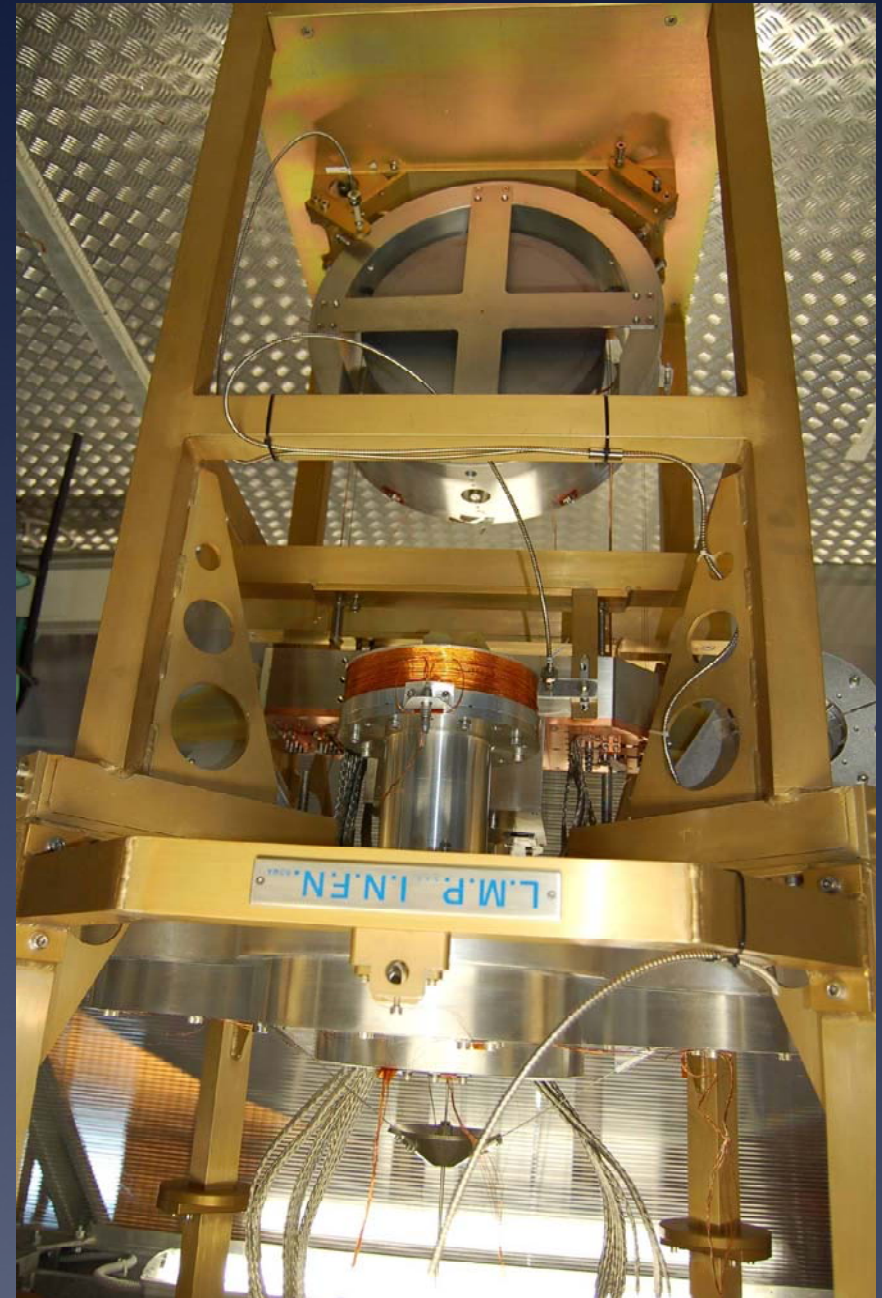
$$\Rightarrow T_{mirror} = 11 \text{ K}$$



# The "cryo last stage"

## Set-up:

- Silicon mirror suspended by using two copper wires loops;
- Marionette with copper clamps, connected to the cooler by copper heat links, suspended with a titanium alloy cable;
- Reaction mass of the mirror and marionette position monitored with fiber bundle sensors to measure the system modes (suspended with copper wires);
- Reaction mass of the marionette holding the Virgo-like electromagnetic actuators (macor support, copper wire kapton insulated);
- MRM suspended with three titanium wires;

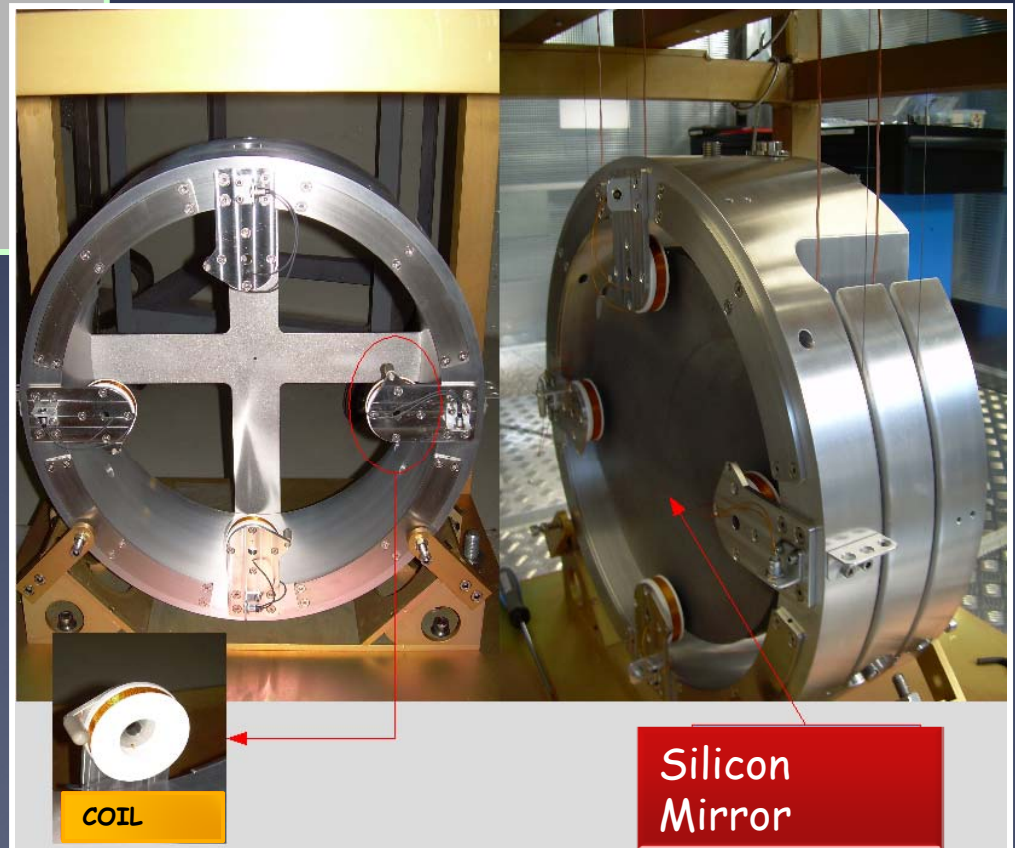


# Marionetta RM and Mirror RM



Silicon Mirror and its RM

Suspension System of the payload and MRM

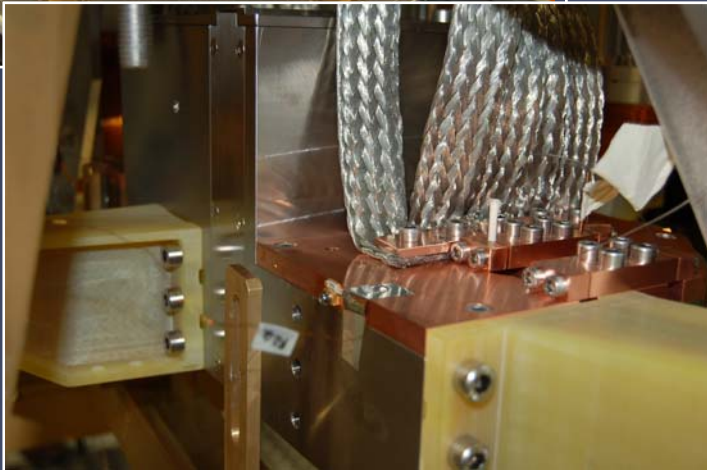
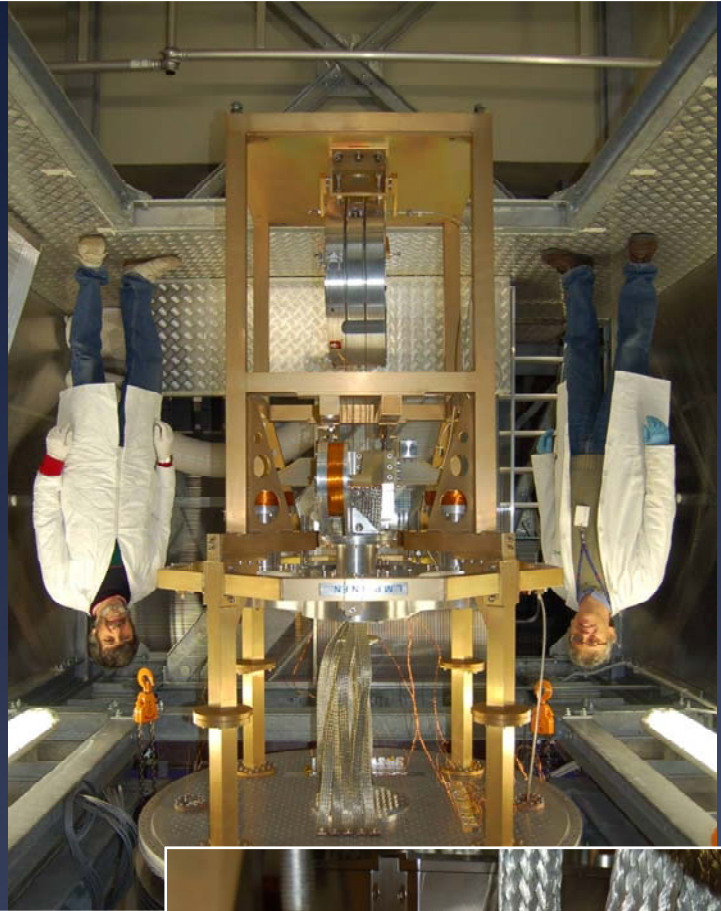


COIL

Silicon Mirror



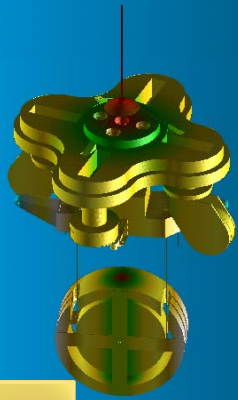
## Thermal links



## Fiber bundle sensors

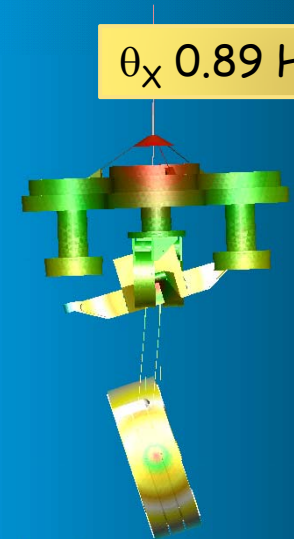
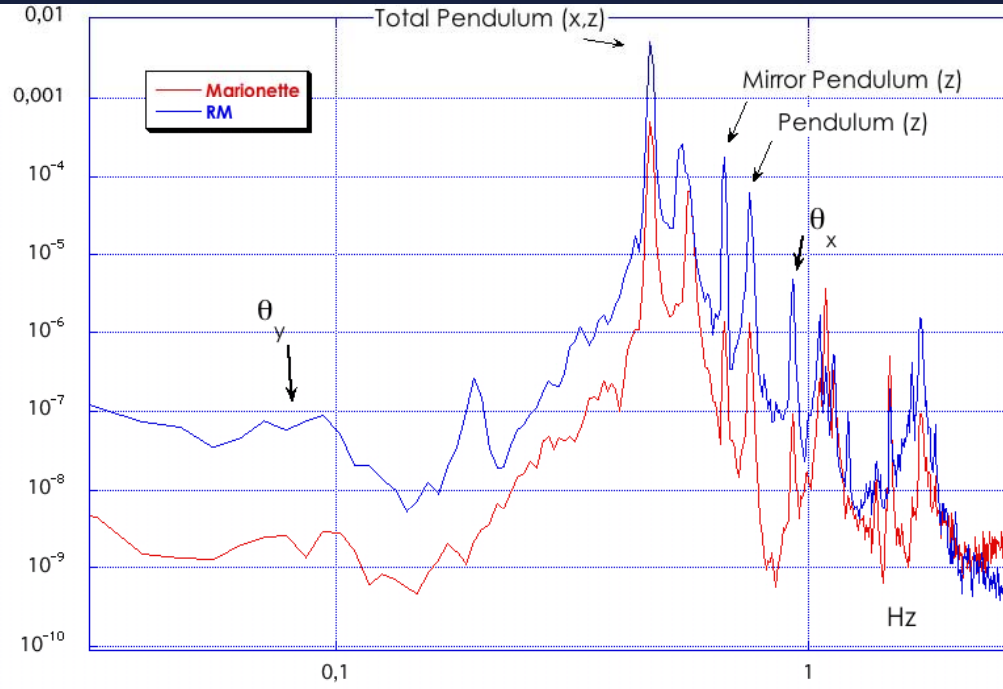


# Study of the mechanical behavior (I)



$\theta_y$  88mHz

Cryogenic Payload

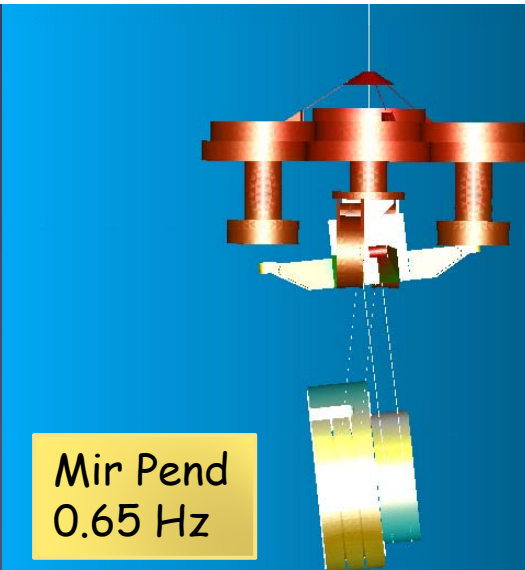


$\theta_x$  0.89 Hz

Cryogenic Payload

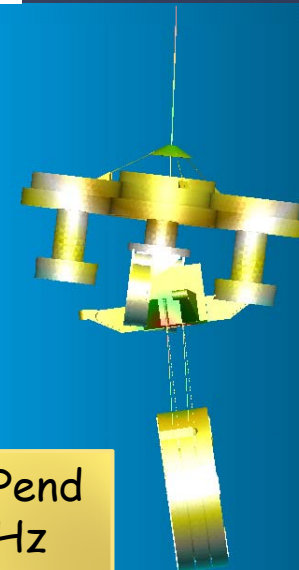


Total Pend  
0.48 Hz



Mir Pend  
0.65 Hz

Cryogenic Payload

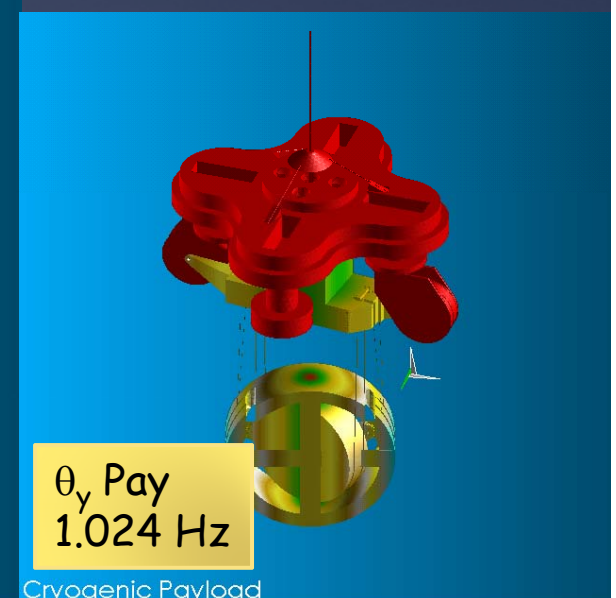
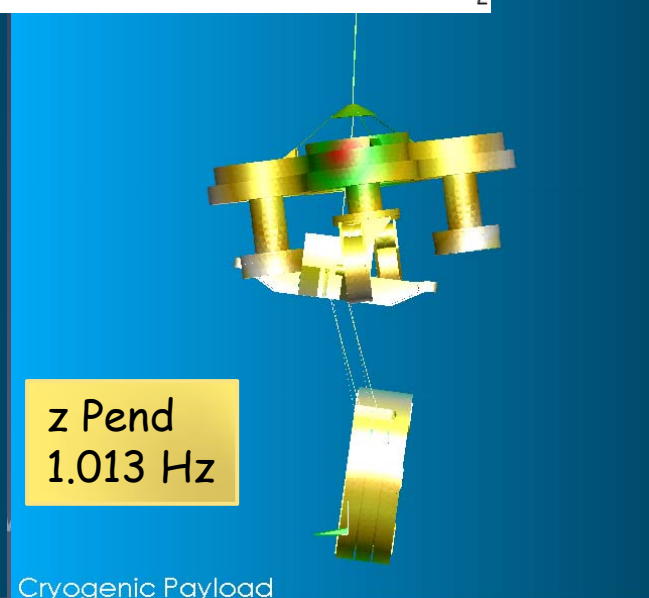
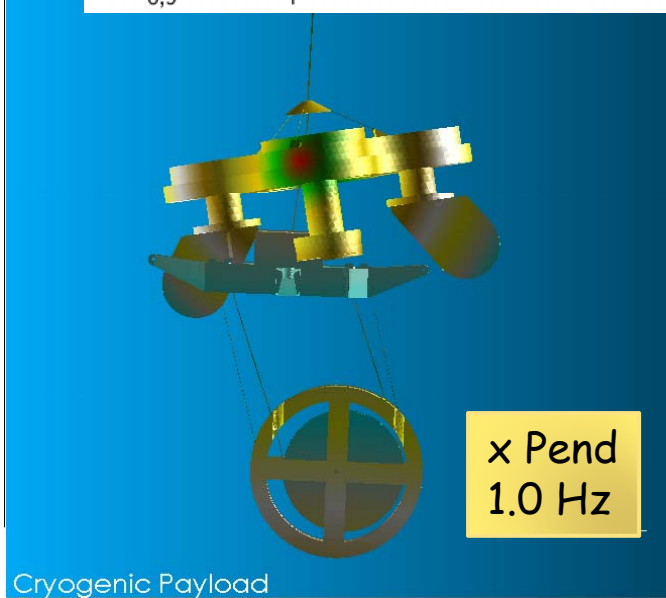
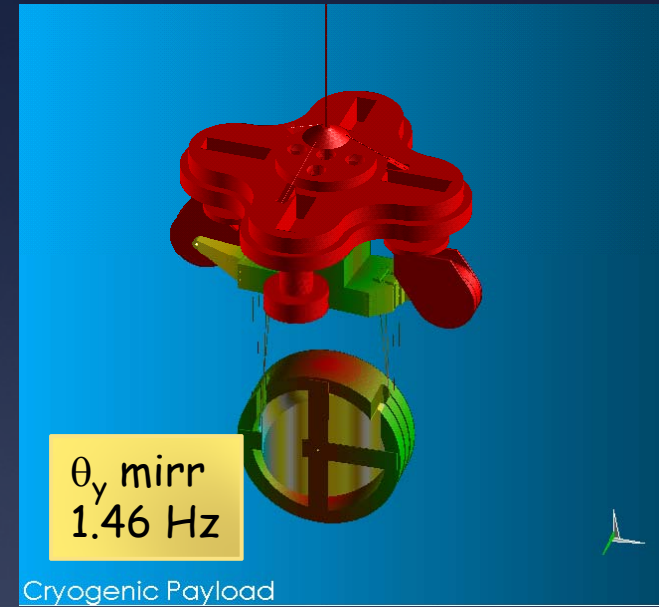
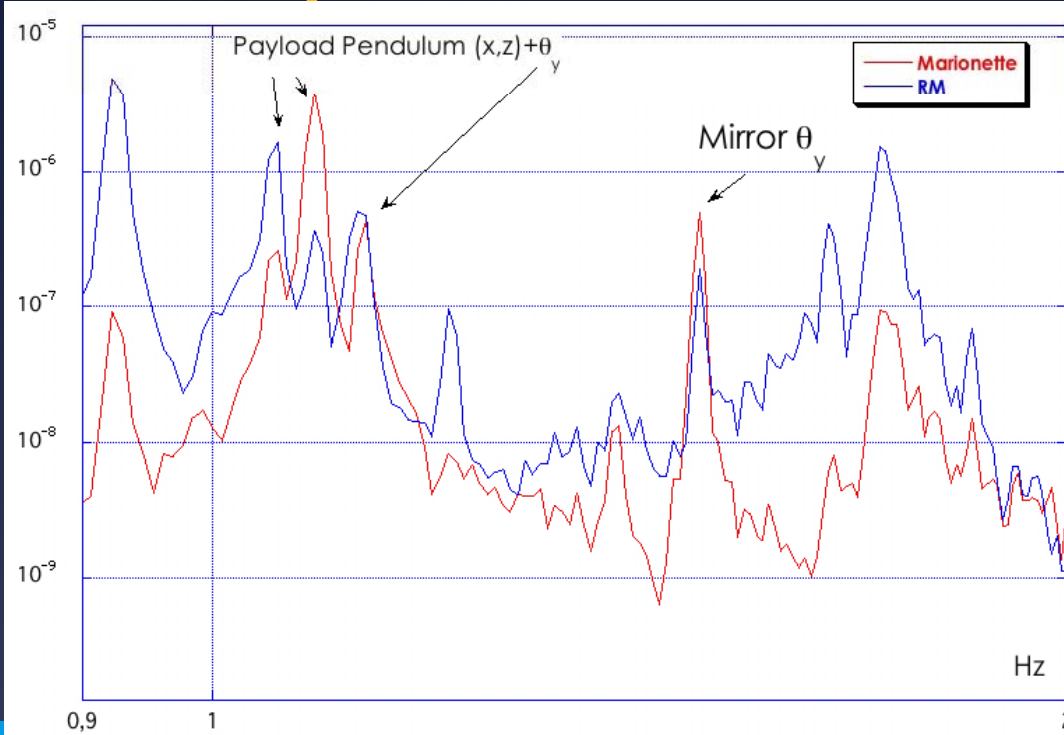


PAY Pend  
0.71 Hz

Cryogenic Payload

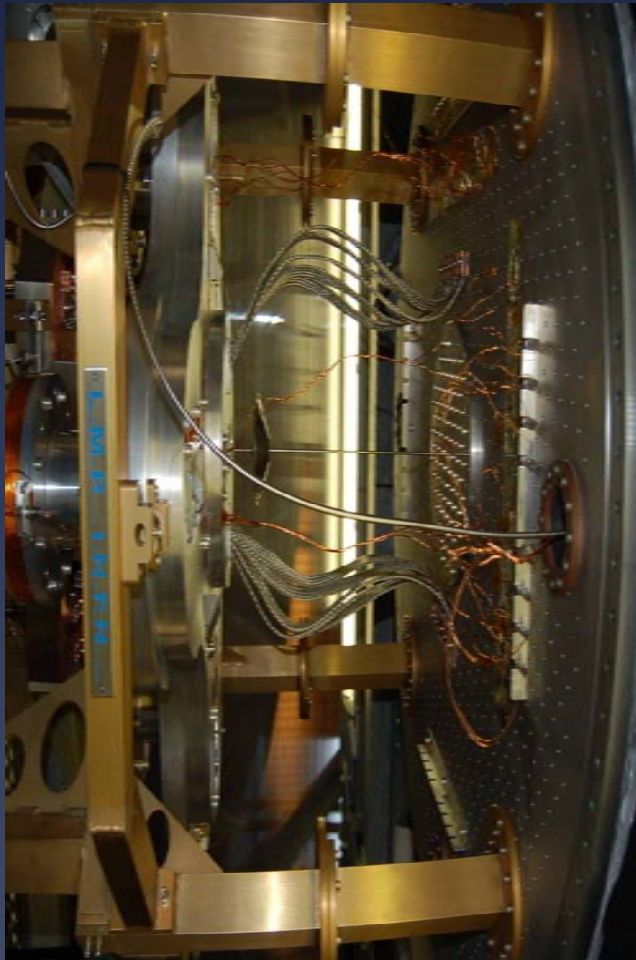


# Study of the mechanical behavior (II)

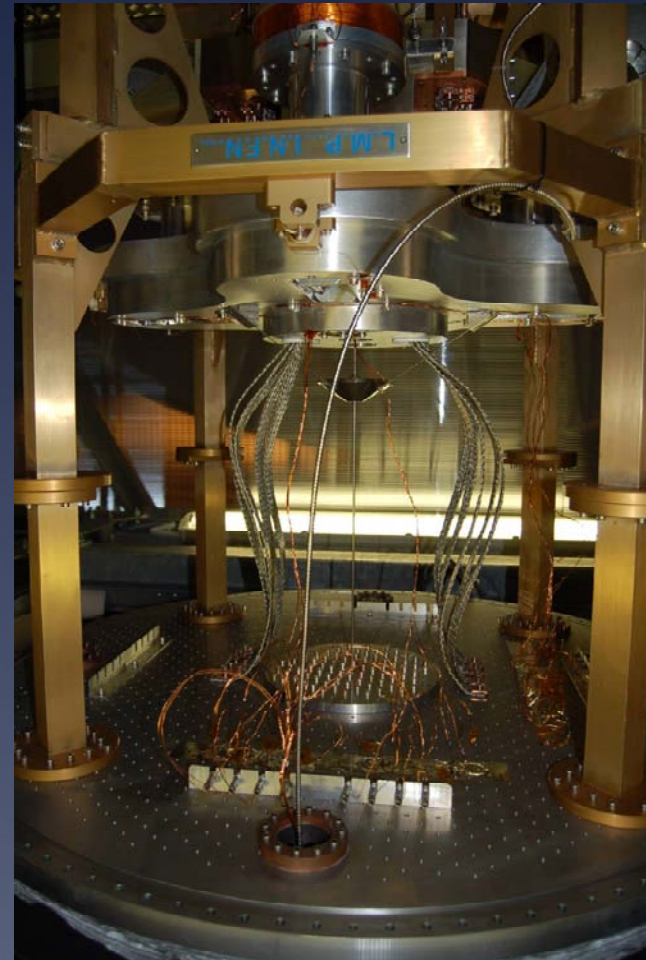


Last week the system was inserted in the cryostat (On Virgo site 1500WA)  
the cooling has started

Ready for insertion



Closed Vacuum chamber





# Status and next steps of the last stage cryogenic payload

## Present

- ▣ The last stage cryogenic payload was characterized mechanically
- ▣ It is being cooled down;

## Very Near Future

- ▣ Measurement of the thermal behavior at low temperature of the new payload .
- ▣ Monitor the system frequencies at low temperature.

*Improvement of the design of the cryo payload and its cooling system*