

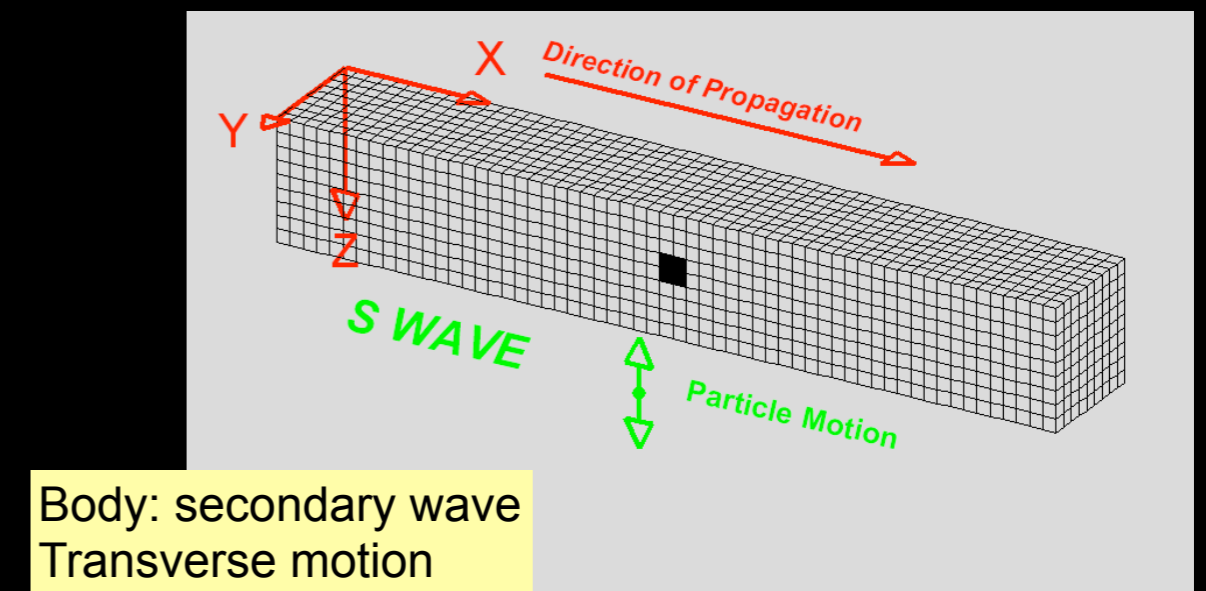
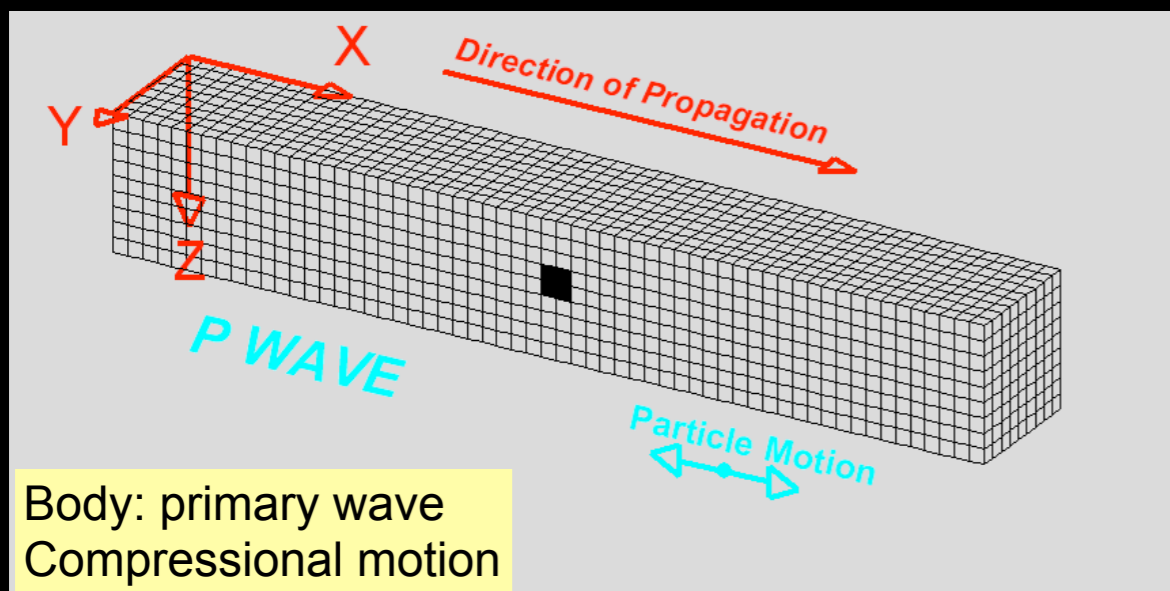
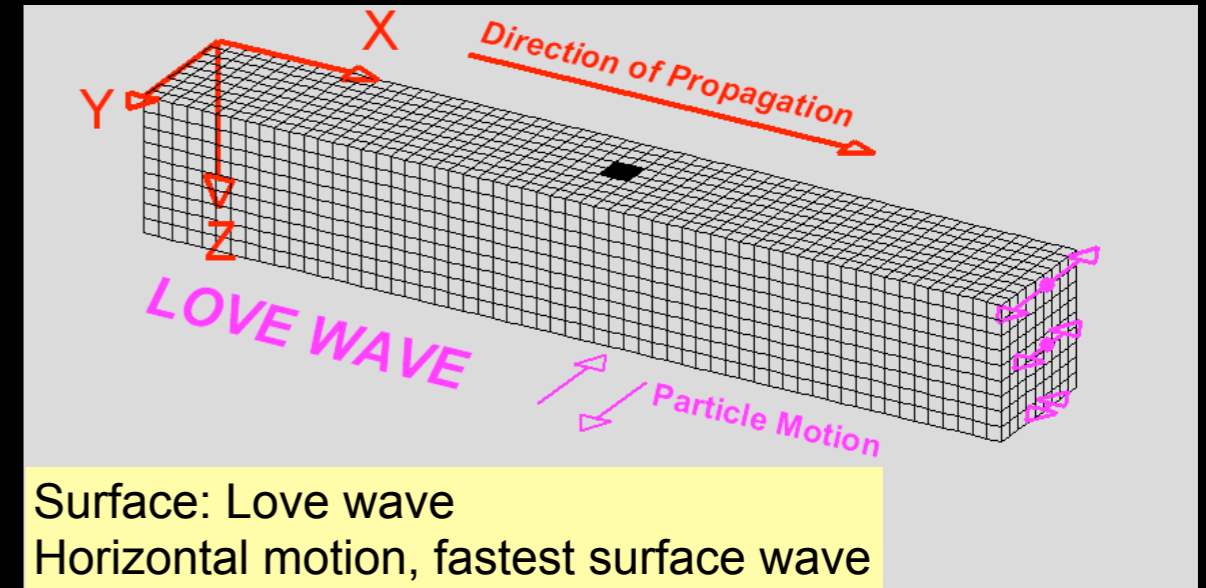
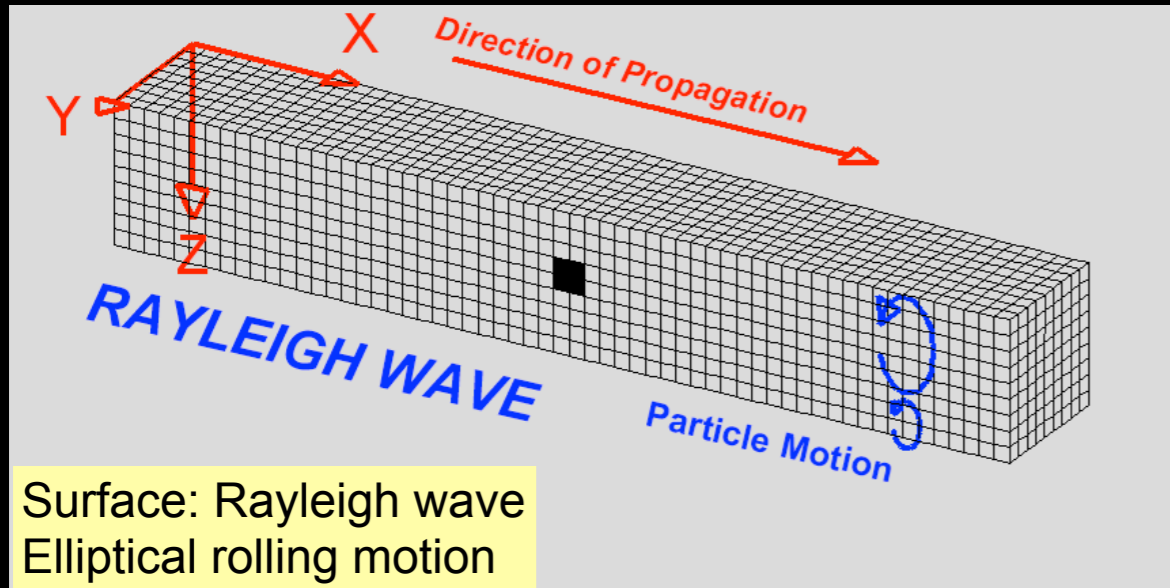
Finite element calculations
of
gravity gradient noise
for
subterranean gravitational wave detectors

16 October 2009
Mark Beker
2nd ET Workshop Erice

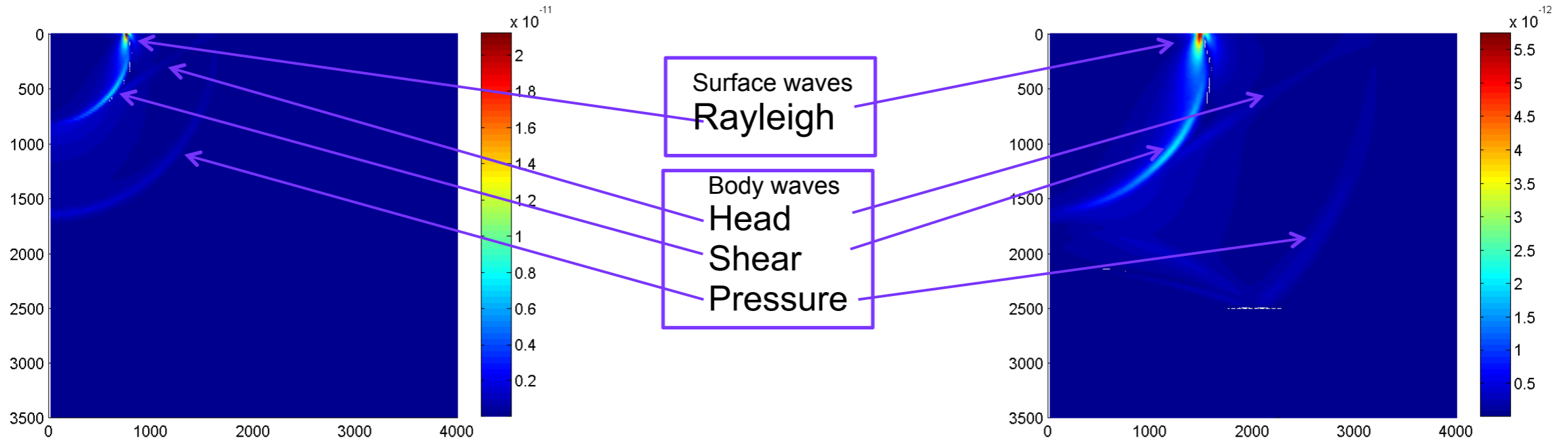
Why we need finite element simulations for GGN

- FEA provide solutions to the wave equation
- Solutions to the wave equation constitute various wave types
 - *Surface: Rayleigh, Love waves*
 - *Body: Pressure, Shear, Head waves*
- Allows to simulate realistic geologies
 - *Multi-layer systems*
 - *Faults / reflections / scattering centers*
- Can be used to test and verify subtraction algorithms

Solutions to the wave equation include surface and body waves

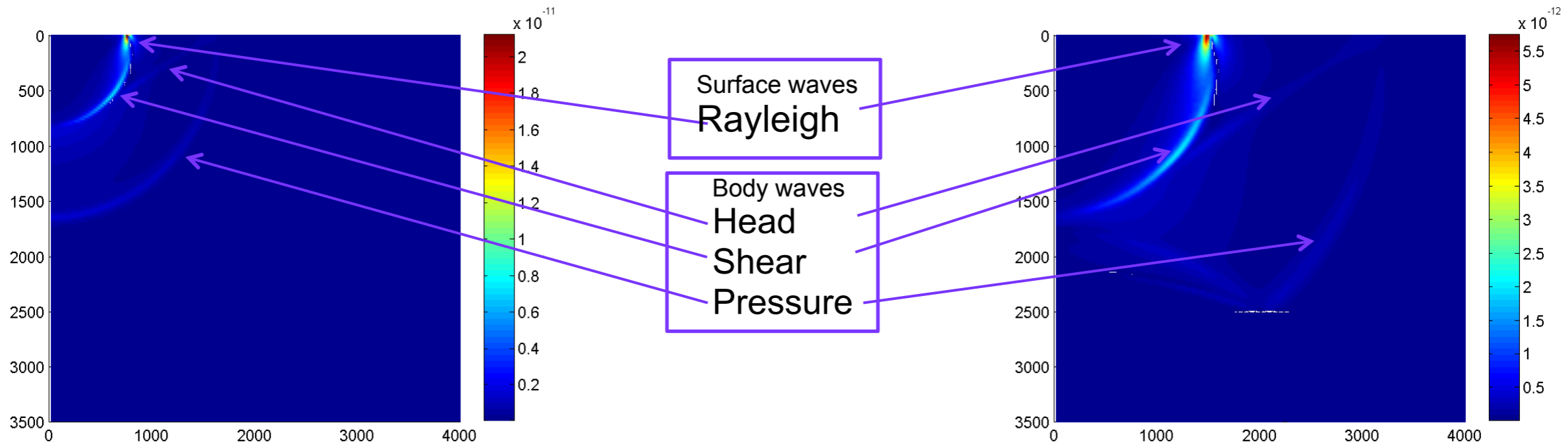


Finite element solutions for all wave fields



- Reaction to vertical point oscillation
 - Two layer geology
- Wave attenuation has two components
 - Geometrical (expansion of wave fronts) $\sim r^n$
 - Rayleigh, $n=-1/2$
 - Body waves at depth, $n=-1$
 - Material (damping)

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$$A_r = \frac{A_o}{\sqrt{r/r_o}} \exp\{-\pi f r / c Q\}$$

then $1/Q = \alpha c / \pi f = 2\delta f / f$

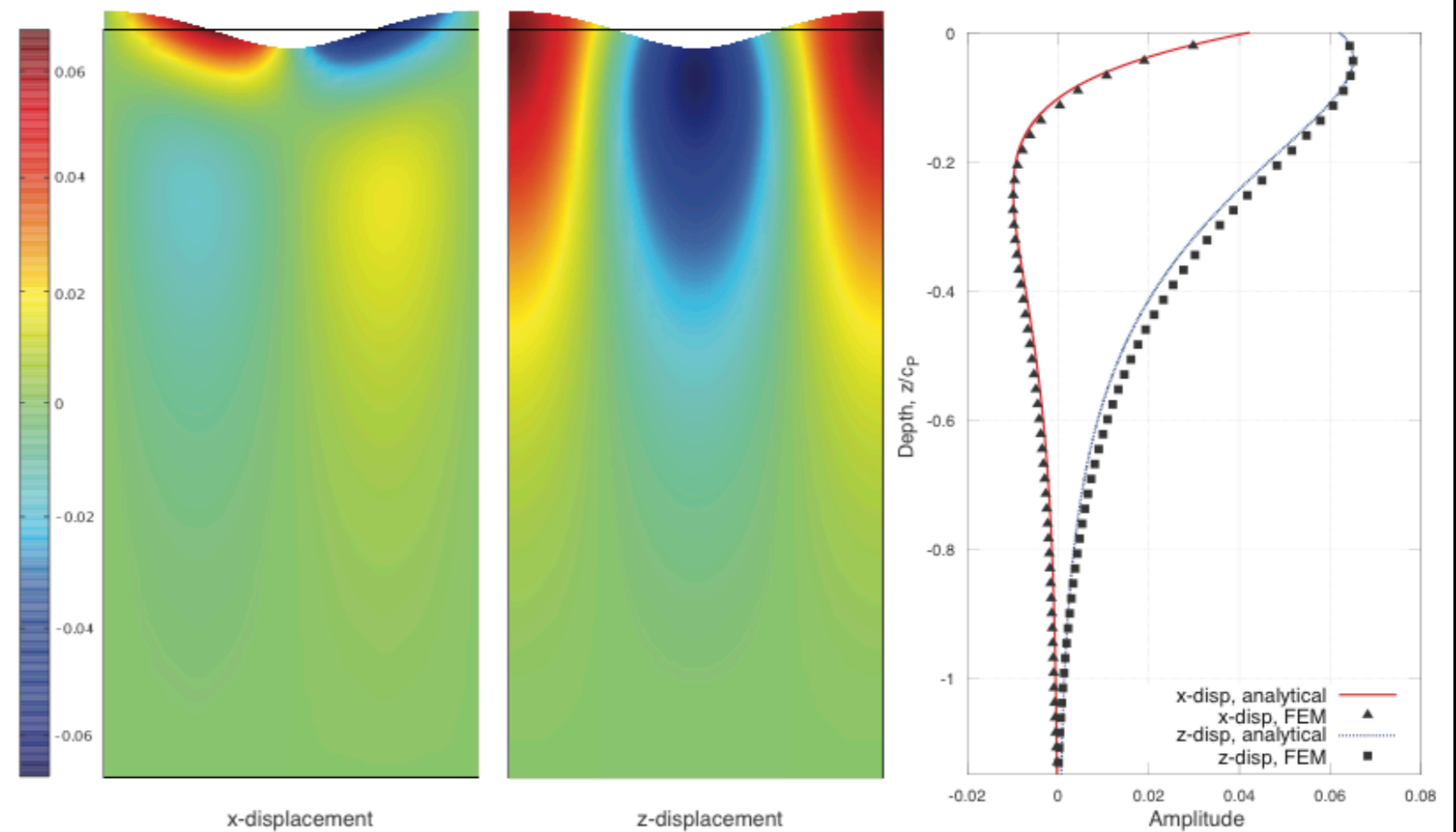
in which c = velocity ,
 f = frequency
 α = attenuation/ l
 δf = half width at .707 response

Example: sandstone, $\alpha = 3.5 \times 10^{-8} f \text{ sec/cm}$, a plane wave disturbance at 1 Hz would be attenuated over 10 km by less than 4%

FE models are good approximations of wave equation solutions - can be compared to analytical results

$$\xi_x = Ac_R \left[e^{-\sqrt{c_R^2 - c_P^2}z} - \frac{2\sqrt{(c_R^2 - c_P^2)(c_R^2 - c_S^2)}}{c_S^2} e^{-\sqrt{c_R^2 - c_S^2}z} \right] e^{i(cx - \omega t - \frac{\pi}{2})}$$

$$\xi_z = A\sqrt{c_R^2 - c_P^2} \left[e^{-\sqrt{c_R^2 - c_P^2}z} - \frac{2c_R^2}{2c_R^2 - c_S^2} e^{-\sqrt{c_R^2 - c_S^2}z} \right] e^{i(cx - \omega t)}$$

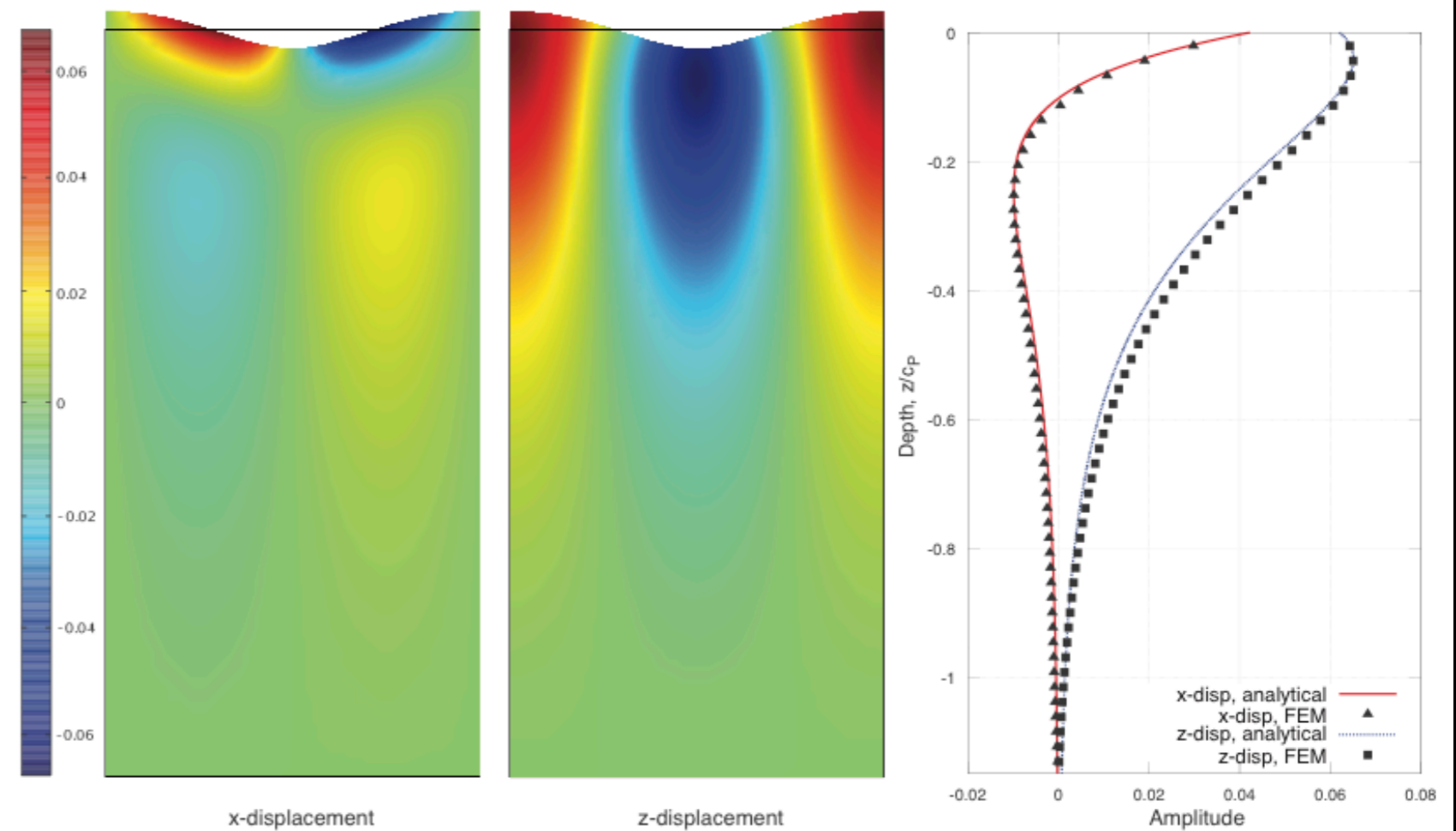


FE models are good approximations of wave equation solutions - can be compared to analytical results

- Rayleigh waves
 - c_R - Rayleigh wave speed
 - c_P/c_S - P/S-wave speed

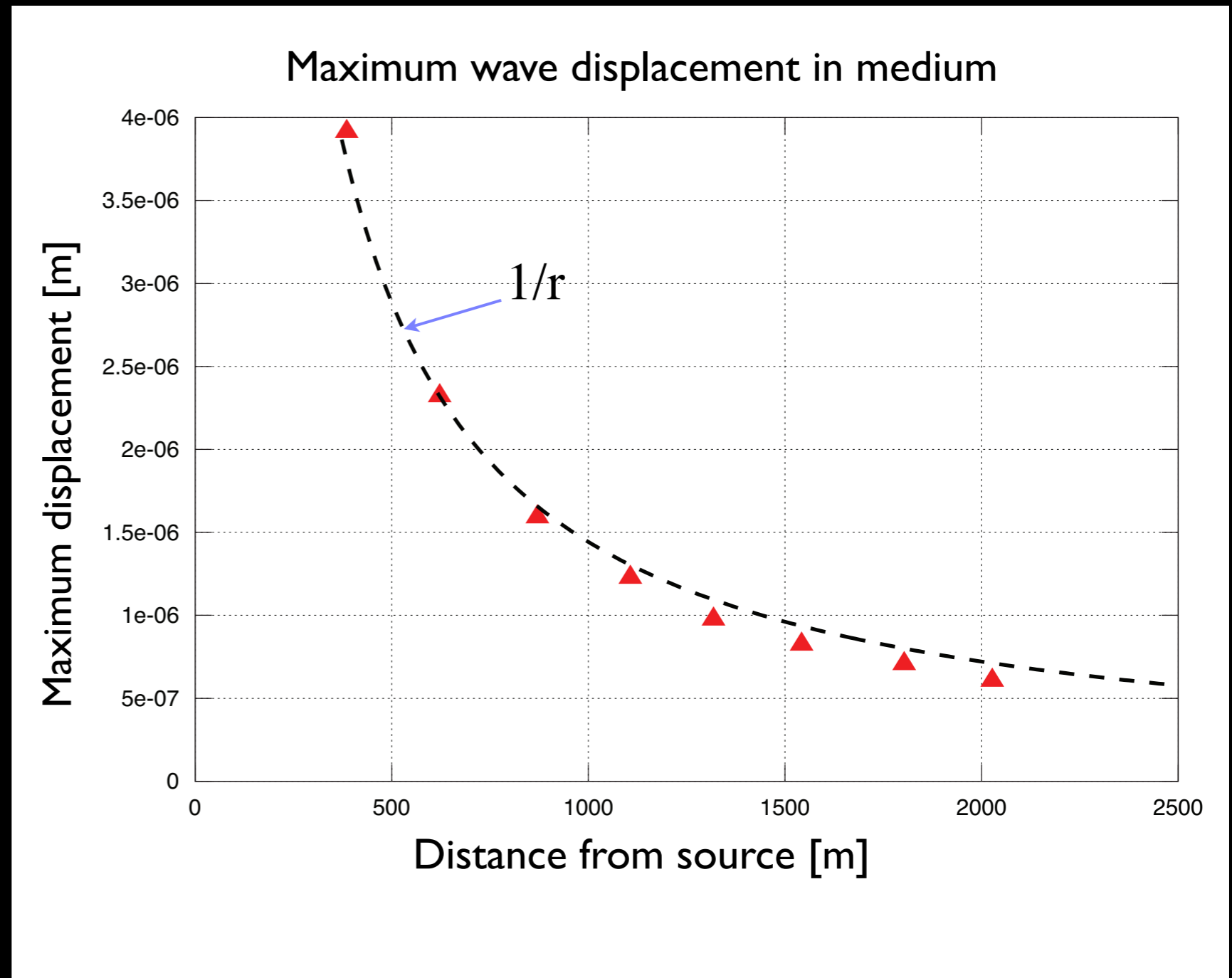
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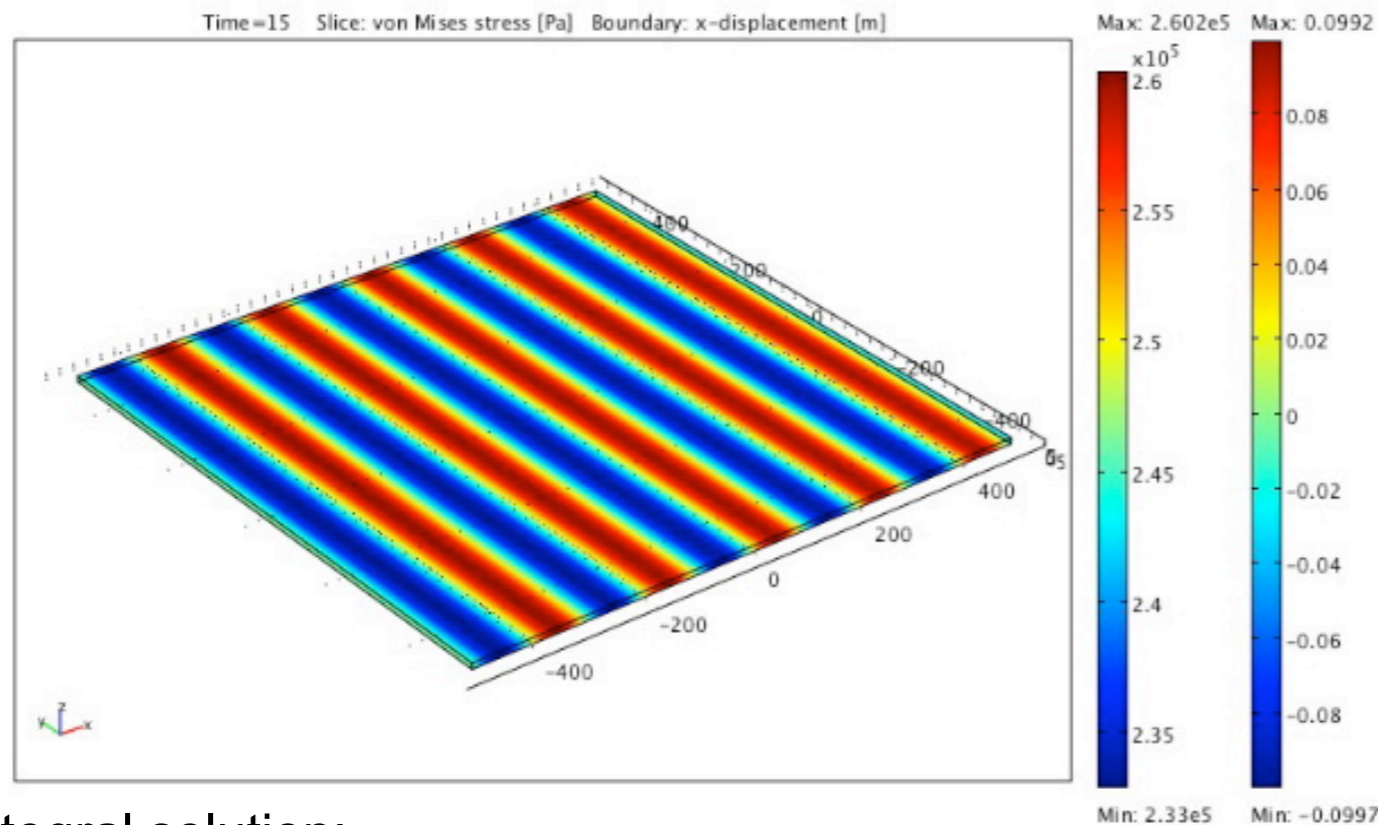
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- Rayleigh waves
 - c_R - Rayleigh wave speed
 - c_P/c_S - P/S-wave speed
- Geometrical damping
 - Body waves in medium $\sim 1/r$
 - Surface waves $\sim 1/rt(r)$



Analytical results are used to verify FE GGN calculations

Homogenous half space as described by Saulson (1984) and Thorne and Hughes (1998)



Plane excited on one side with
 $u(t) = u_0 \cos(\omega t - kx)$
 $u_0 = 0.1 \text{ m}$

Many planes stacked on top of each other to create a block

Like Saulson and Thorne and Hughes an integral lower bound is used ($r_{\text{cut-off}}$) of $\lambda/4$

Ground properties:

$\rho = 1800 \text{ kg/m}^3$

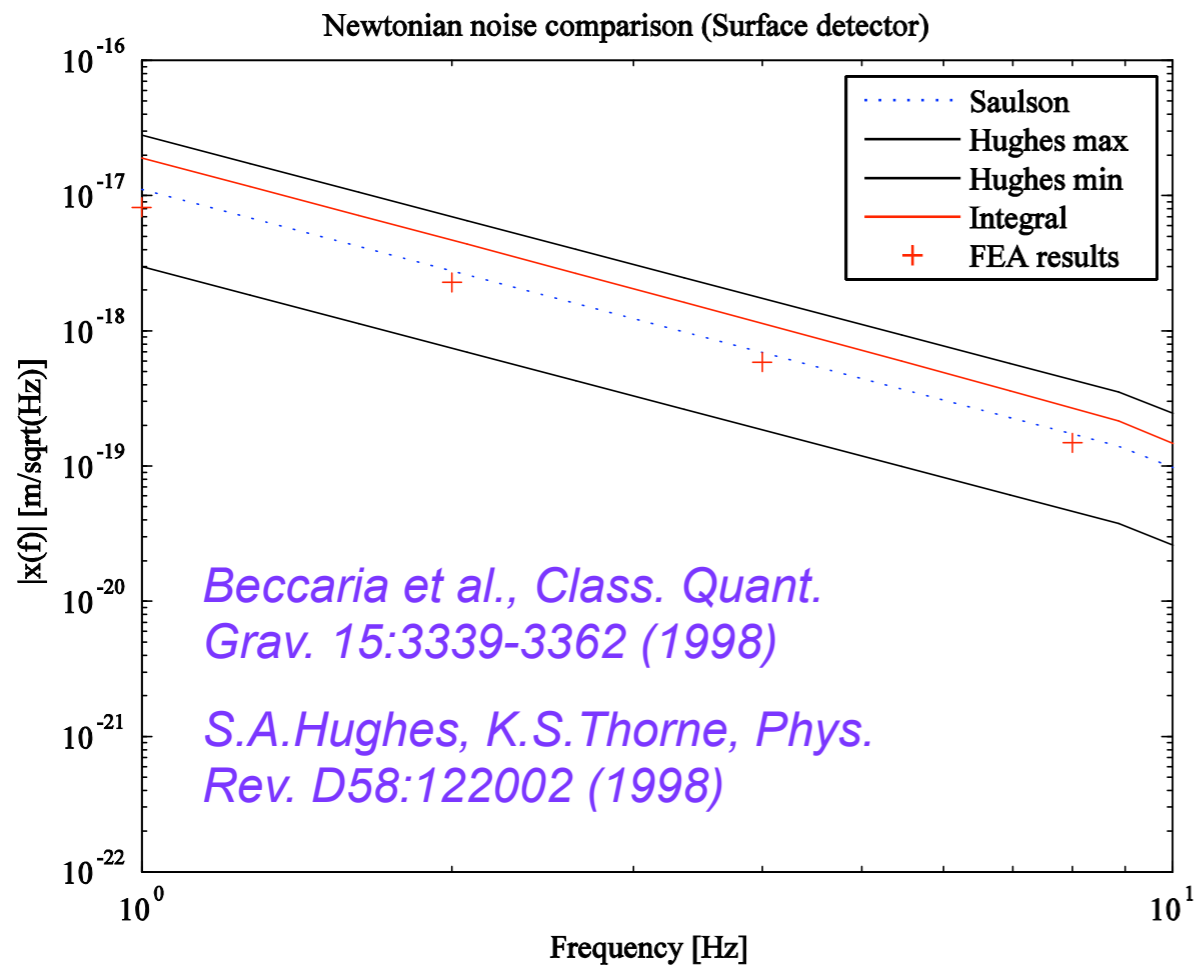
$\nu = 0.33$

$c_p \approx 440 \text{ m/s}$

Integral solution:

$$\begin{aligned}
 a_{x,pwave,max} &= \int_H \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \frac{G\rho u_0}{(x^2 + y^2 + z^2)^{3/2}} \left(1 - \frac{3x^2}{x^2 + y^2 + z^2} \right) \cos(-kx) dx dy dz \\
 &= 2\pi G\rho u_0 e^{-2\pi \frac{H}{\lambda}}
 \end{aligned}$$

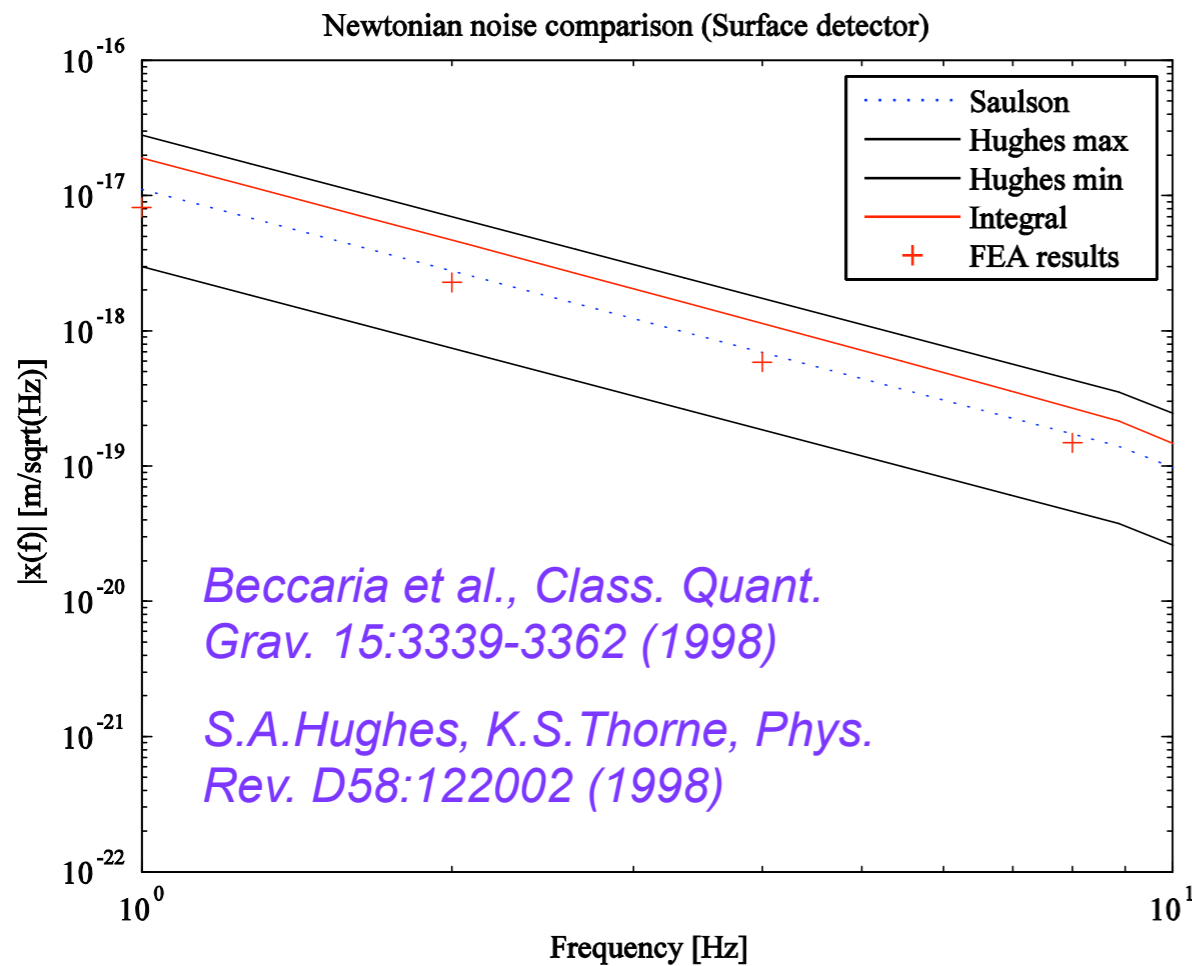
FE calculations show good correspondence with analytical results



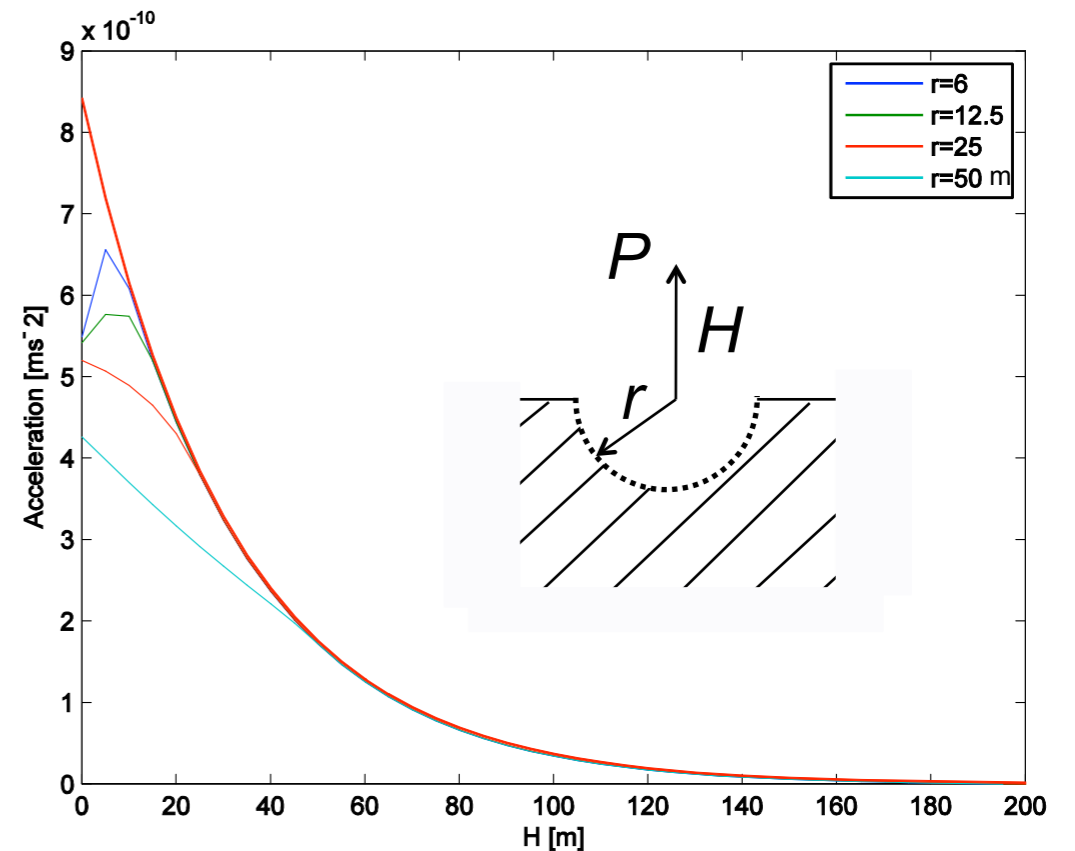
- GGN spectra for surface detectors agree with Saulson, Cella and Hughes
 - For 1 – 10 Hz: 1 nm/rtHz
- Care should be taken regarding element size
- Deviation from integral due to integral cut-off, r



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Reproduction of surface wave calculations - Cella

Analytical results by G. Cella
The 58th Fujihara Seminar
(May 2009)

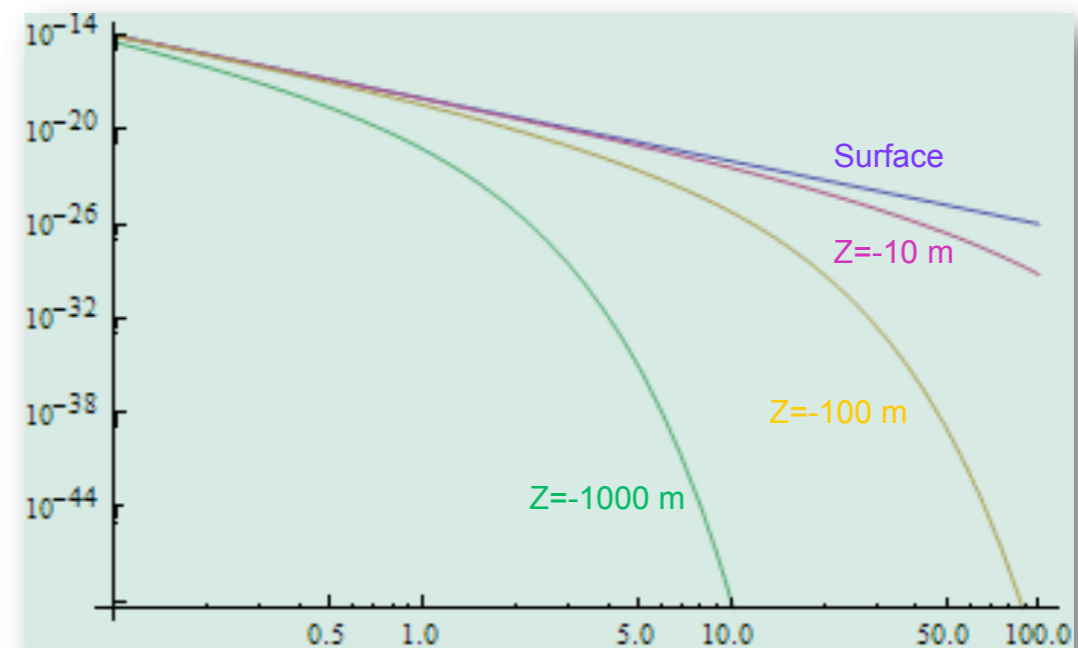
Assumptions:

- $C_p = 1000$ m/s (lower is better)
- $C_p/C_s = 0.5$ (lower is worse)
- Surface modes and transverse mode only
- V/H ratio = $\frac{1}{2}$ (lower is better)

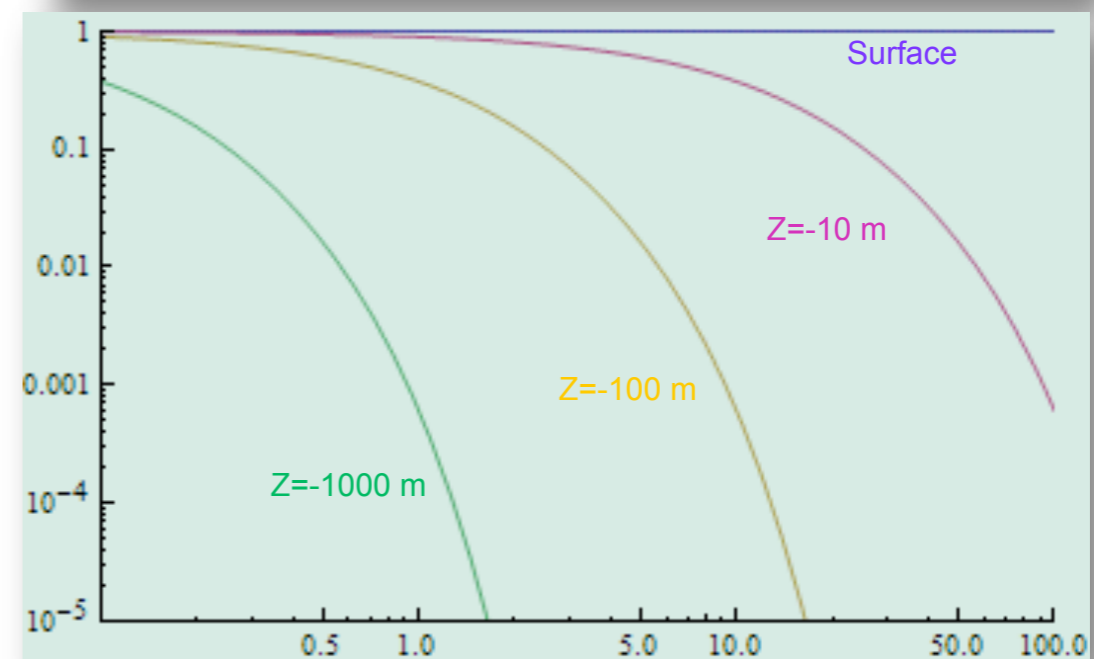
Feasible

- Can we do better?
especially in the low frequency region
- Volume waves!

Equivalent strain noise amplitude (Hz^{-1/2})



GGN reduction factor



Frequency (Hz)

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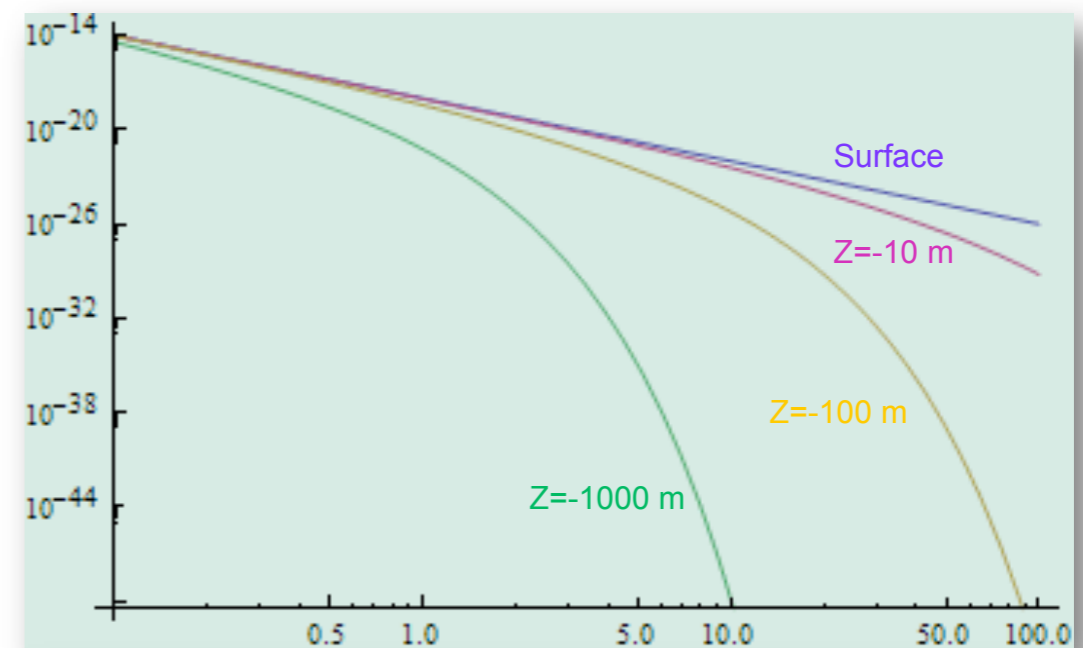
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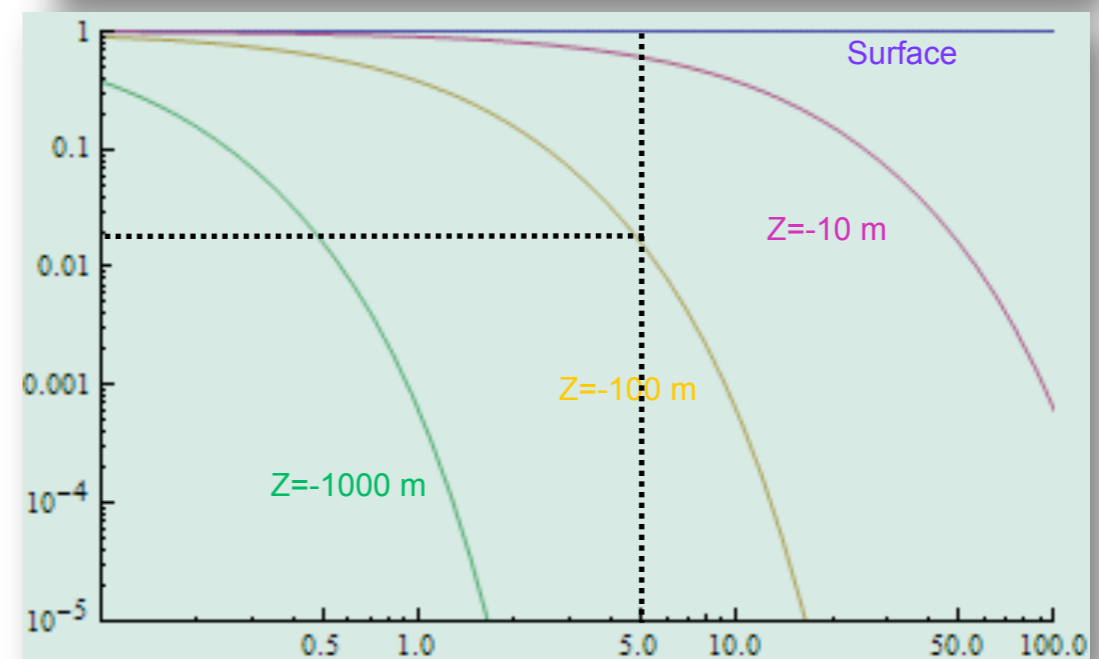
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Reproduction of surface wave calculations - Cella

Double plane wave excitation of surface waves
Soil characteristics to match Cella's calculations

Material properties:

$$E = 1.22 \times 10^9$$

$$\nu = 0.33$$

$$\rho = 1800 \text{ kg/m}^3$$

$$c_p = 1000 \text{ m}$$

$$c_s / c_p = 0.5$$

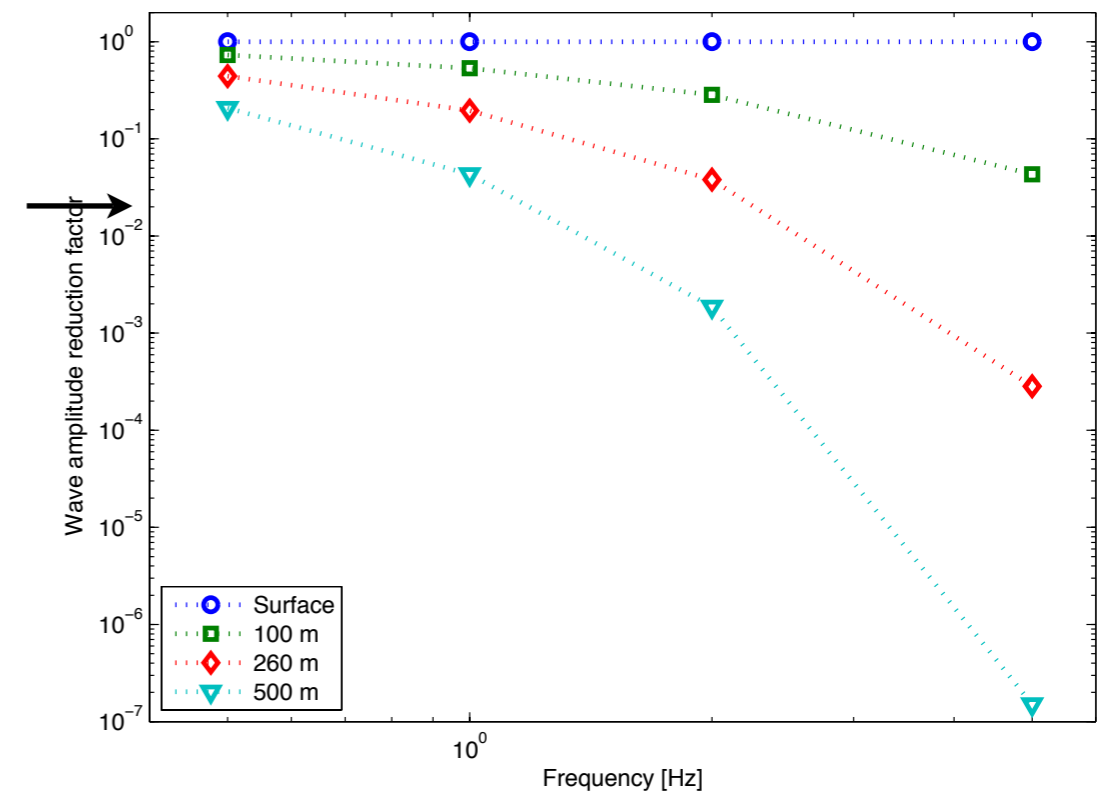
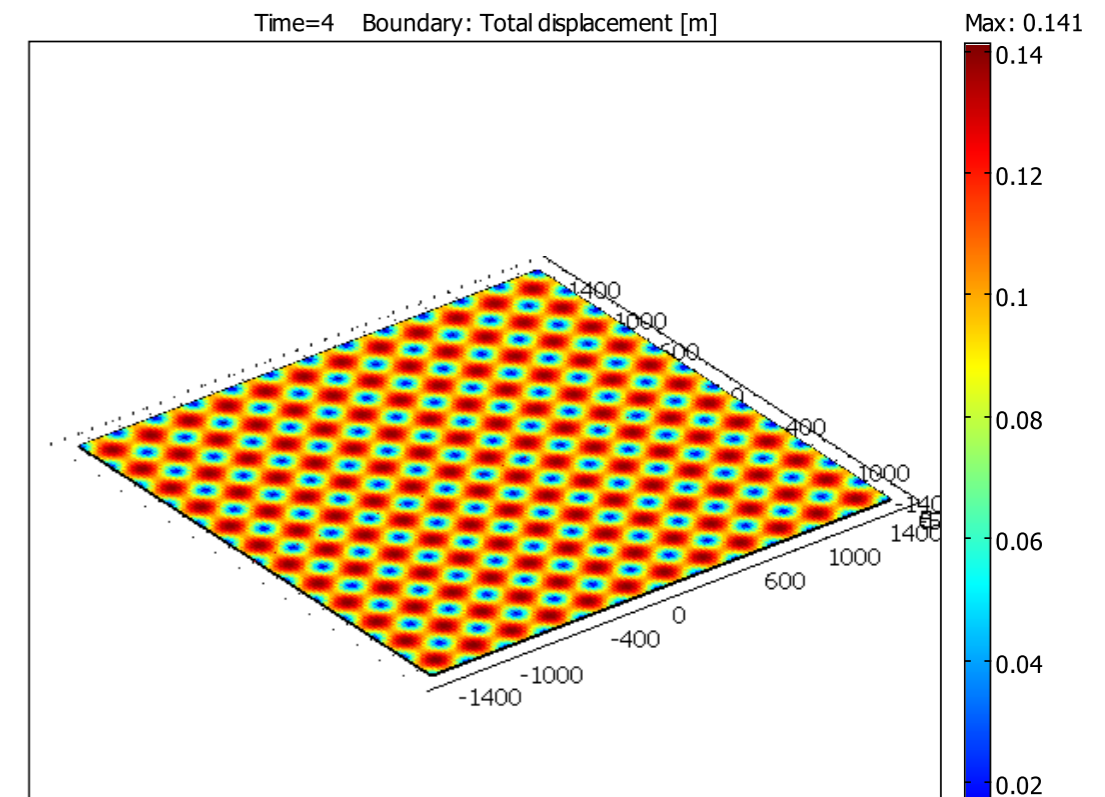
Dimensions:

$$3000 \times 3000 \times 10 \text{ m}$$

Element size:

$$21.4 \times 21.4 \times 10 \text{ m}$$

- Reasonable agreement with Cella
 - Limited model size
 - Deviations at higher frequencies/depths
- Geometric suppression increases with
 - Lower velocities
 - Domination by surface waves
- More realistic model
 - Surface wave amplitudes decay exponentially with depth
 - Include compression waves
 - Include incoherent sources



7

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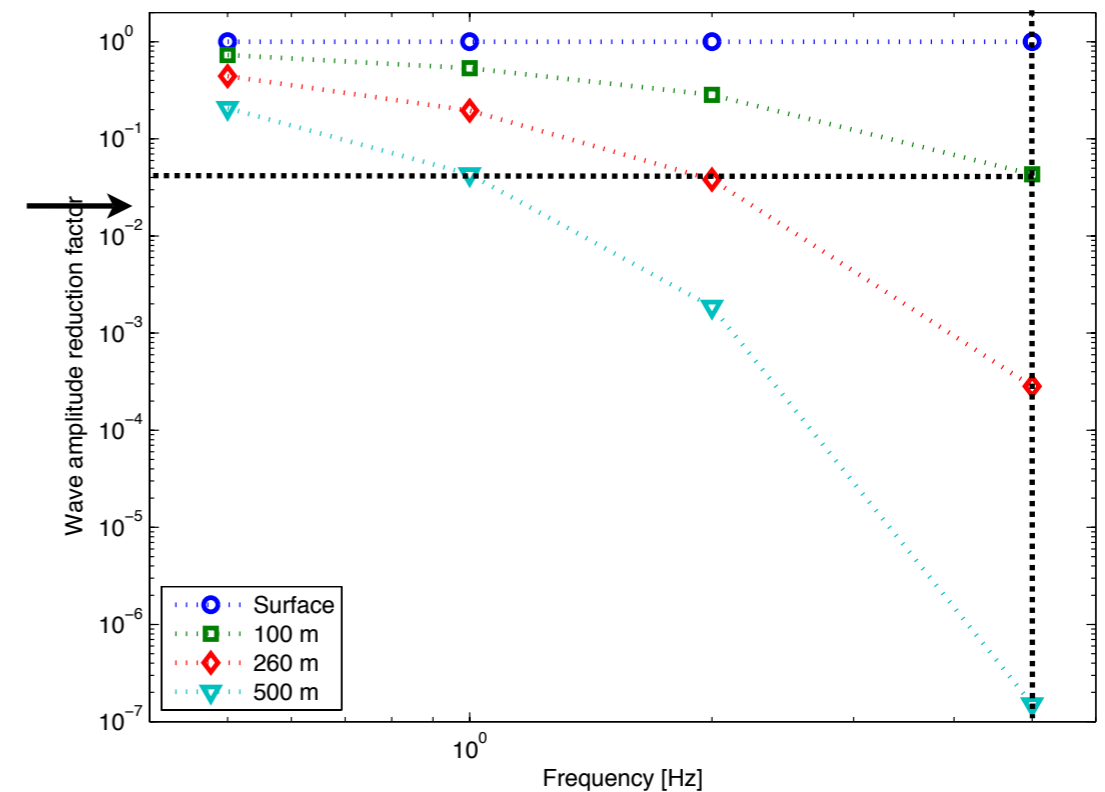
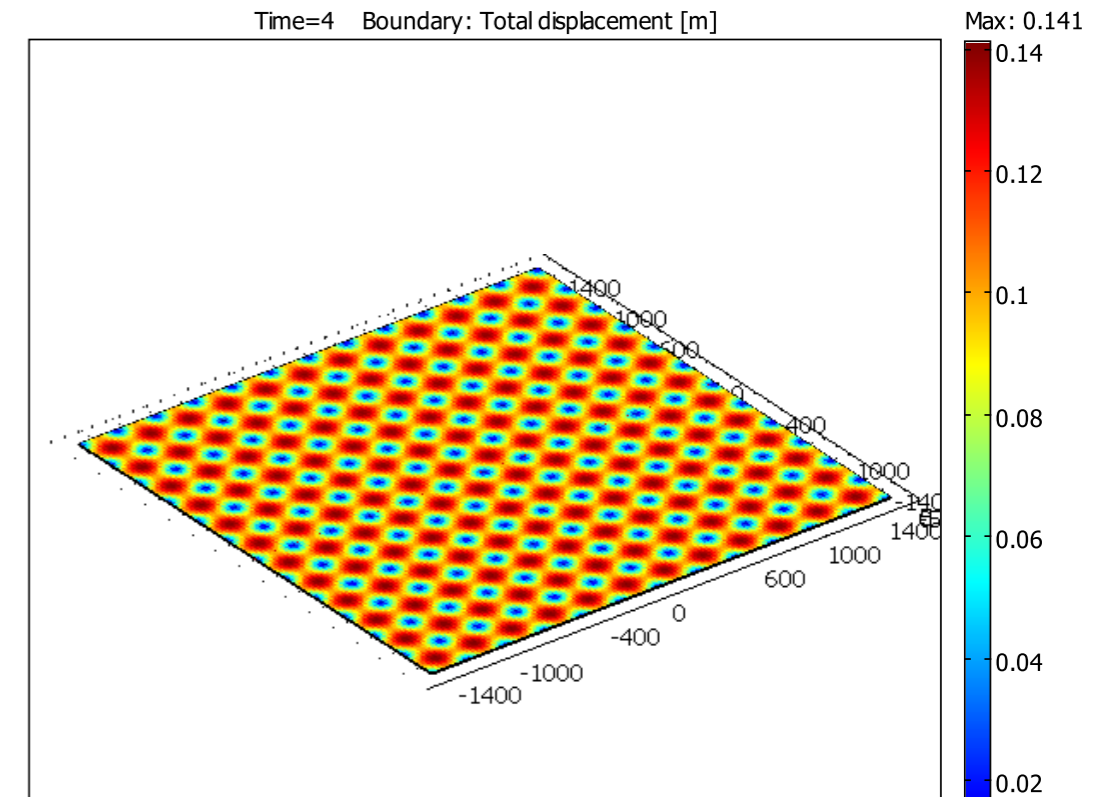
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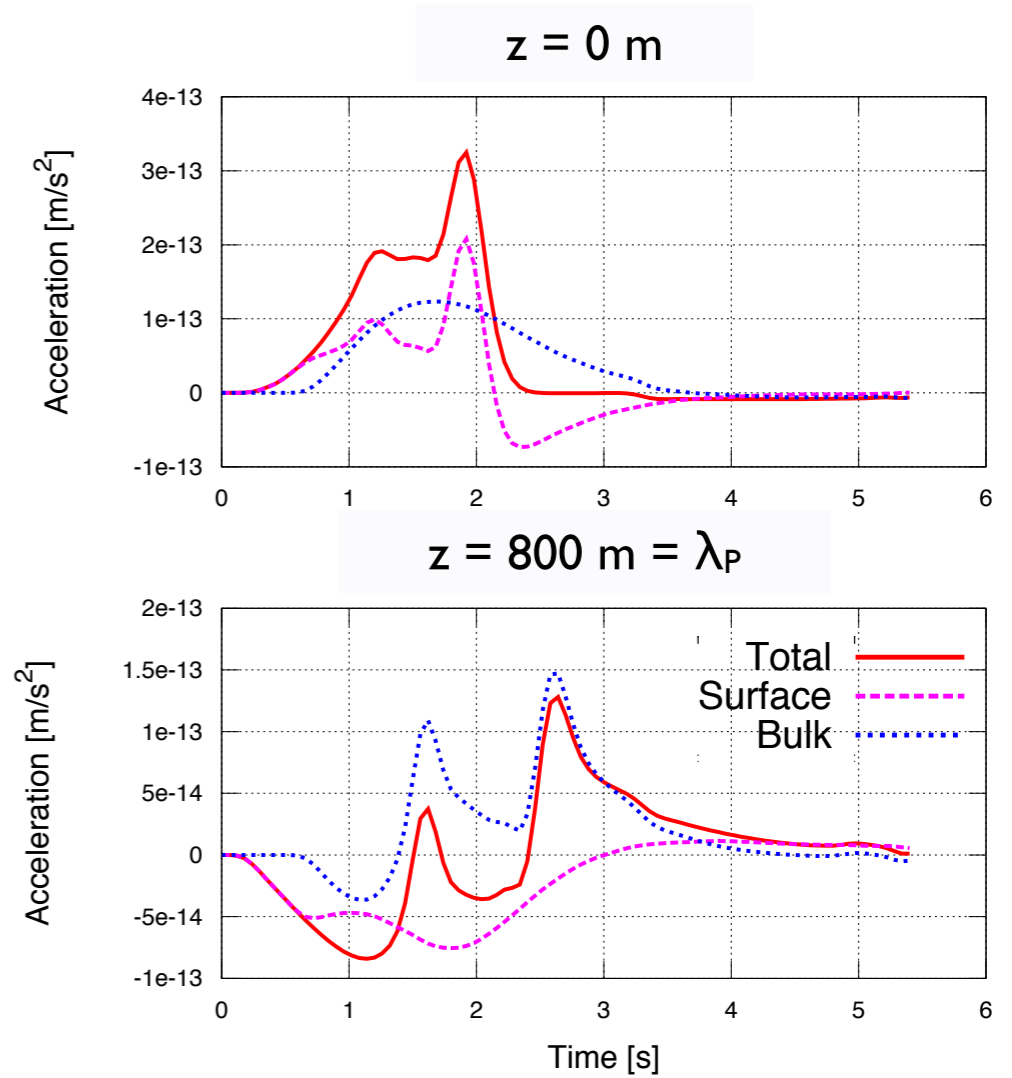
7

ET GGN requirements

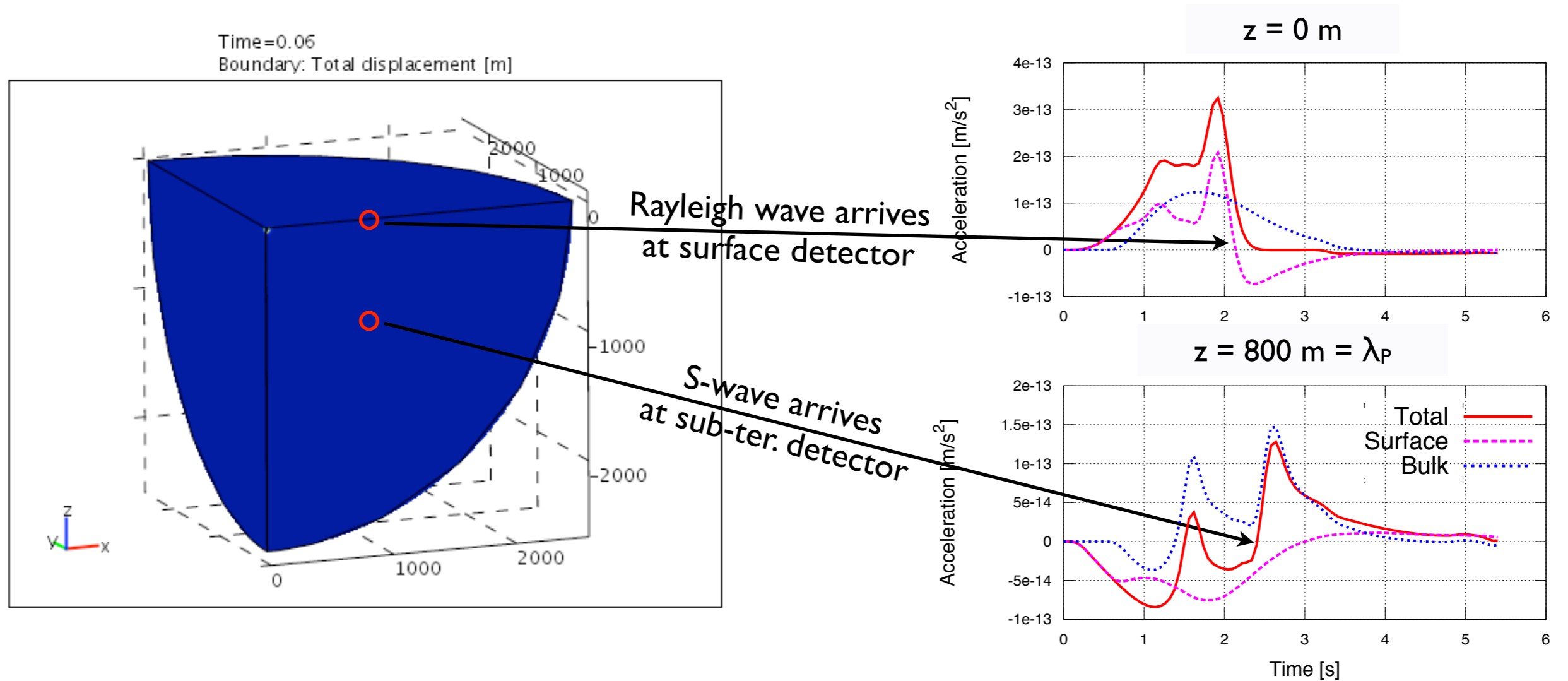
- A reduction factor of 50 is required compared to 5 nm/rtHz
- Surface site with 0.1 nm/rtHz is unrealistic
- Underground: Surface wave averaging may provide significant reduction...
- Cultural noise (pumps / people / traffic) must be minimised
- Investigate effects of cultural noise on gravity gradients

Impulse excitations are used to simulate cultural noise events

-
-

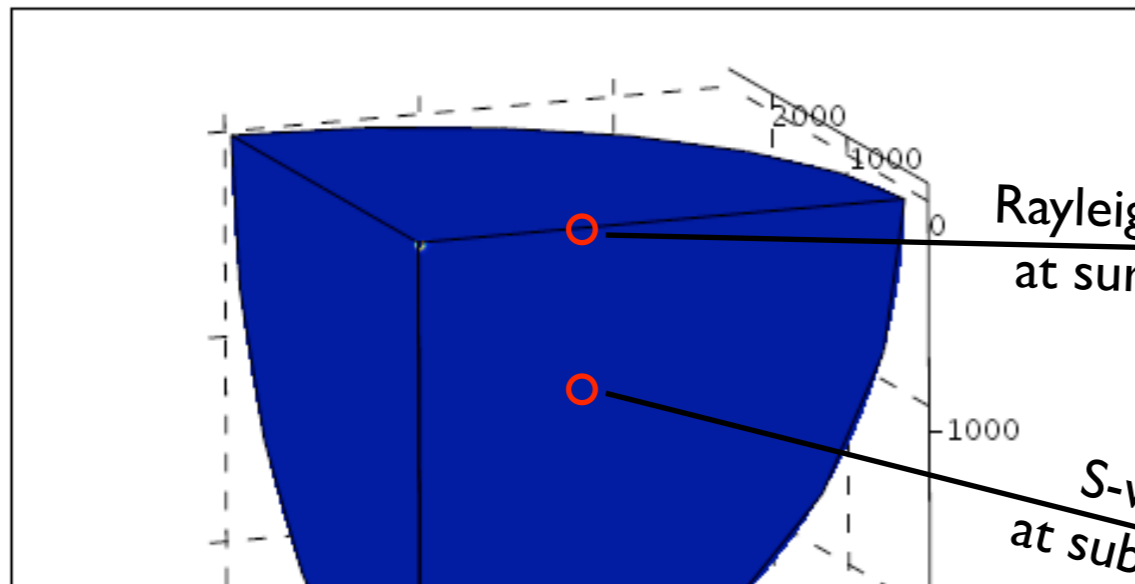


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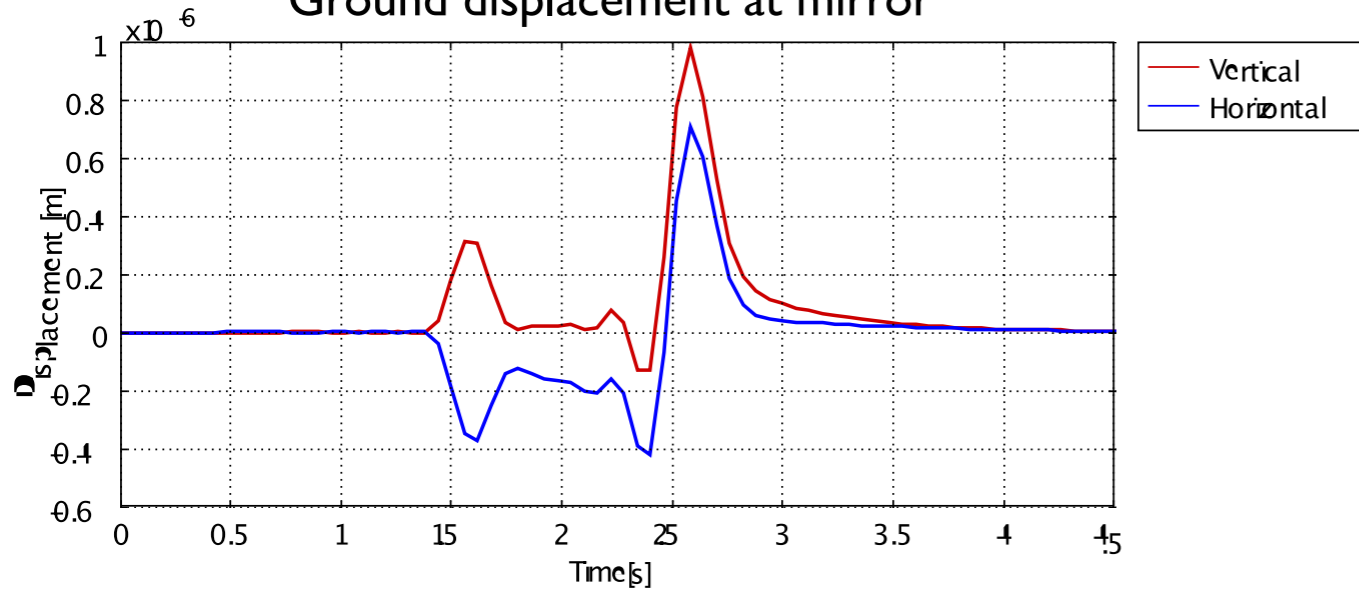
Time=0.06
Boundary: Total displacement [m]



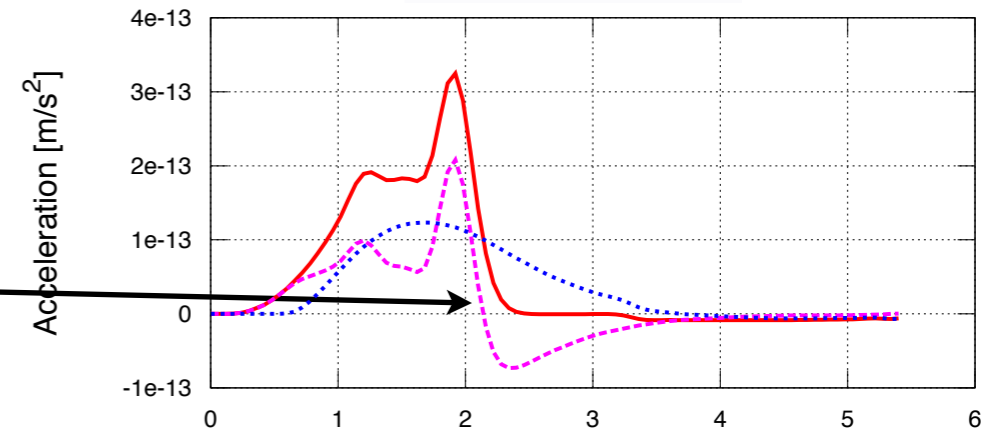
Rayleigh wave arrives at surface detector

S-wave arrives at sub-terranean detector

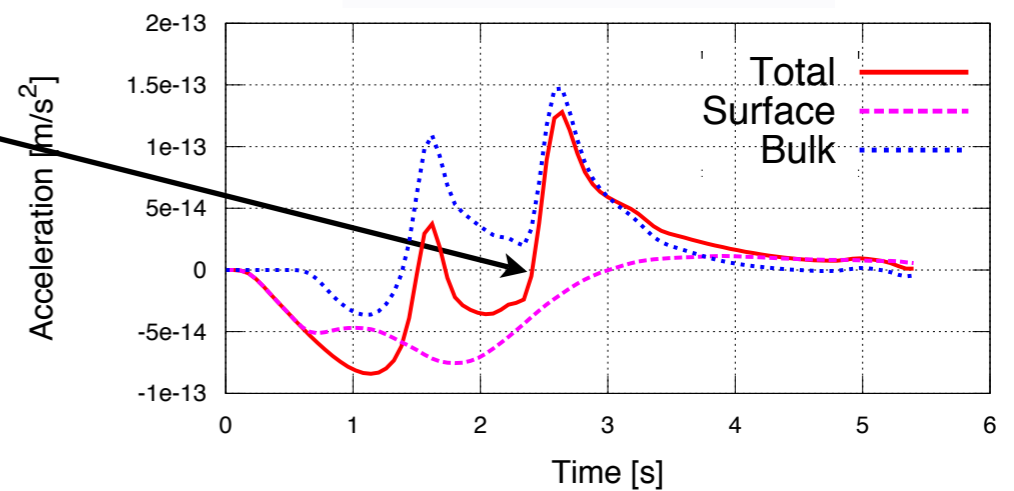
Ground displacement at mirror



$z = 0 \text{ m}$

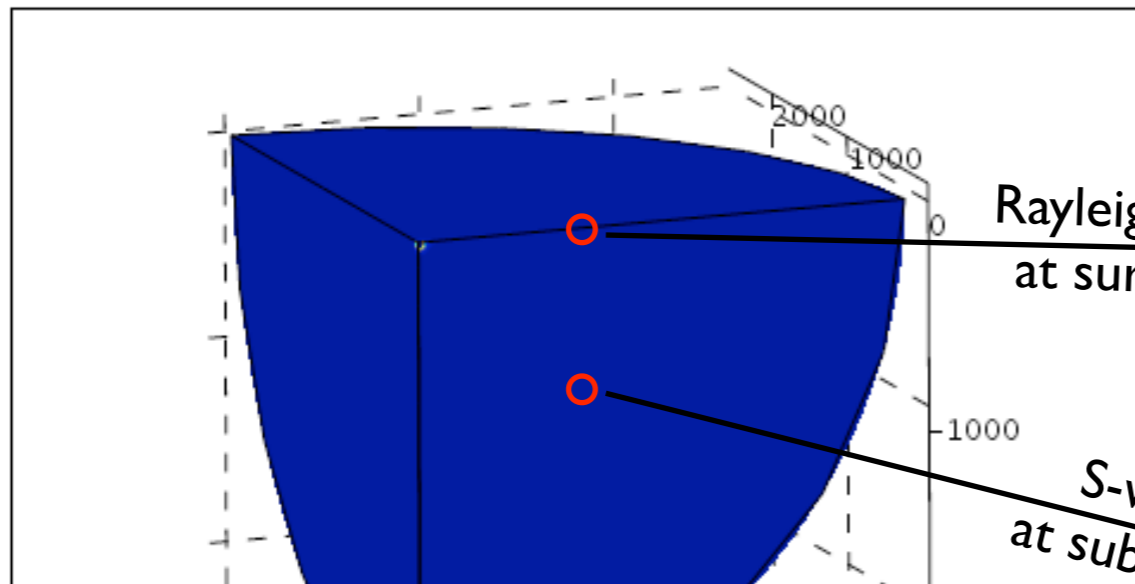


$z = 800 \text{ m} = \lambda_P$



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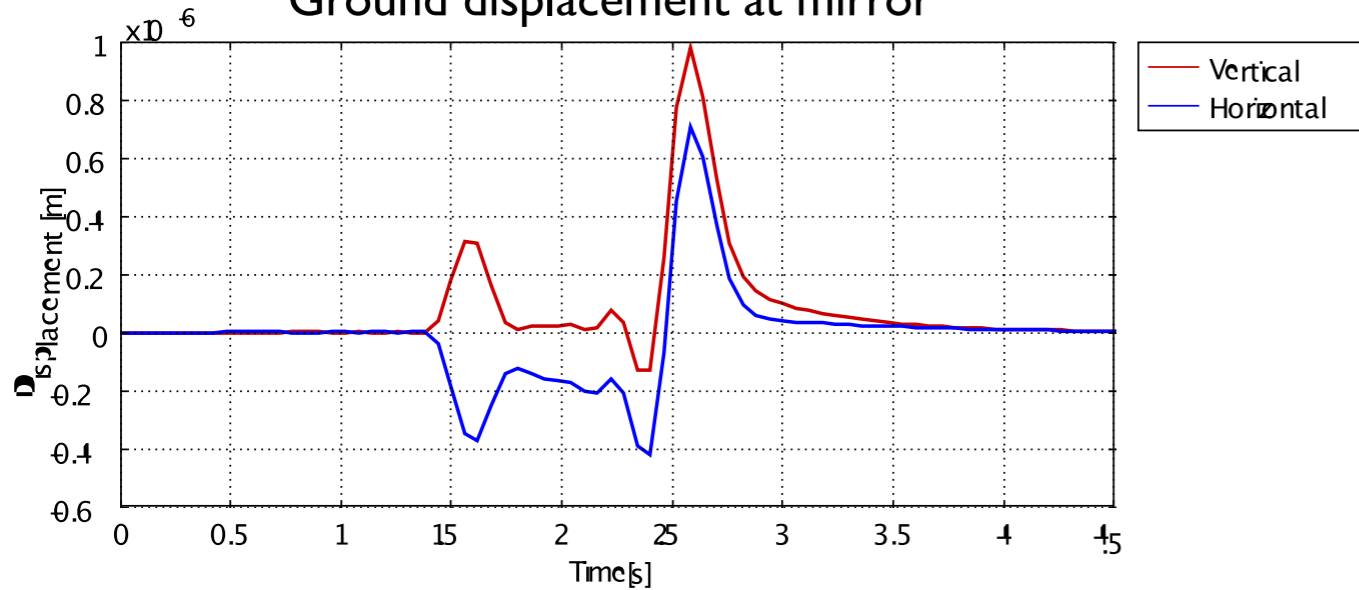
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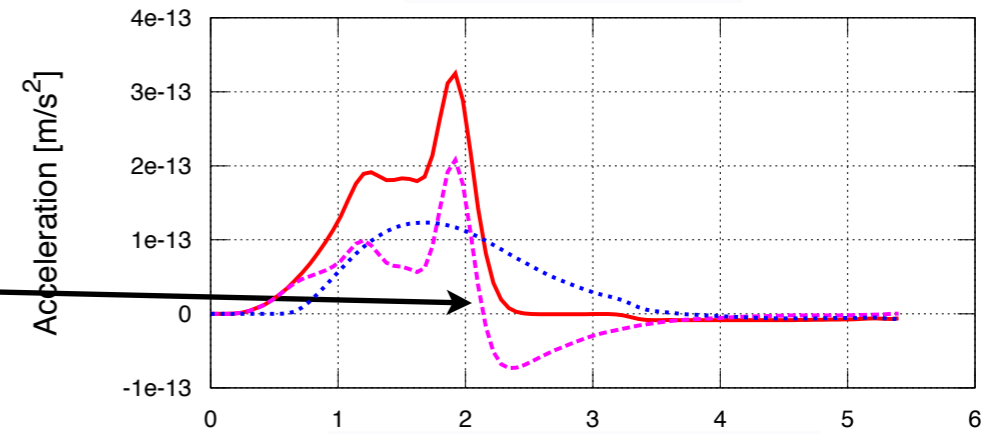
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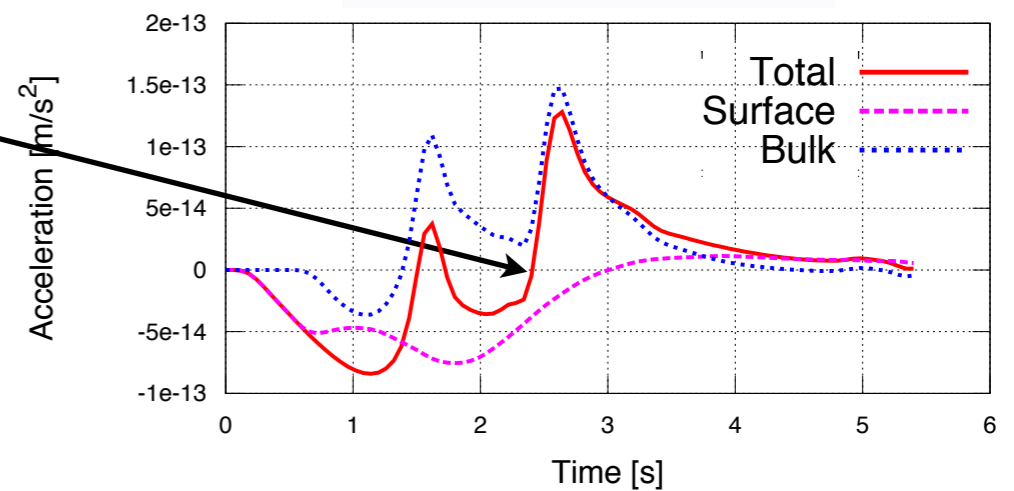
Ground displacement at mirror



$z = 0 \text{ m}$



$z = 800 \text{ m} = \lambda_P$



Reduction factor < 3

Harmonic excitation of a homogenous medium of Clay or Granite



Clay:

$$\lambda_P = 800 \text{ m}$$

$$\lambda_S = 462 \text{ m}$$

$$\rho = 2000 \text{ kg/m}^3$$

$$\nu = 0.25$$

Granite:

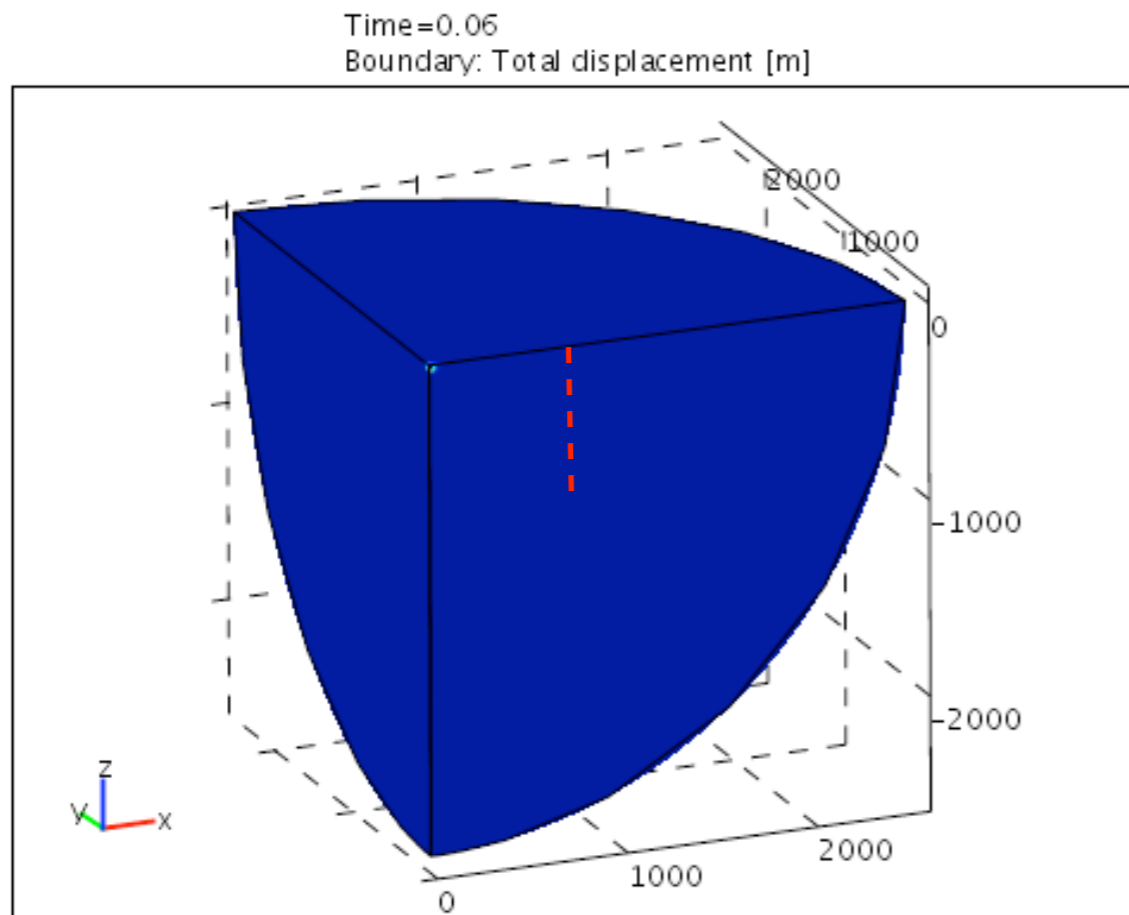
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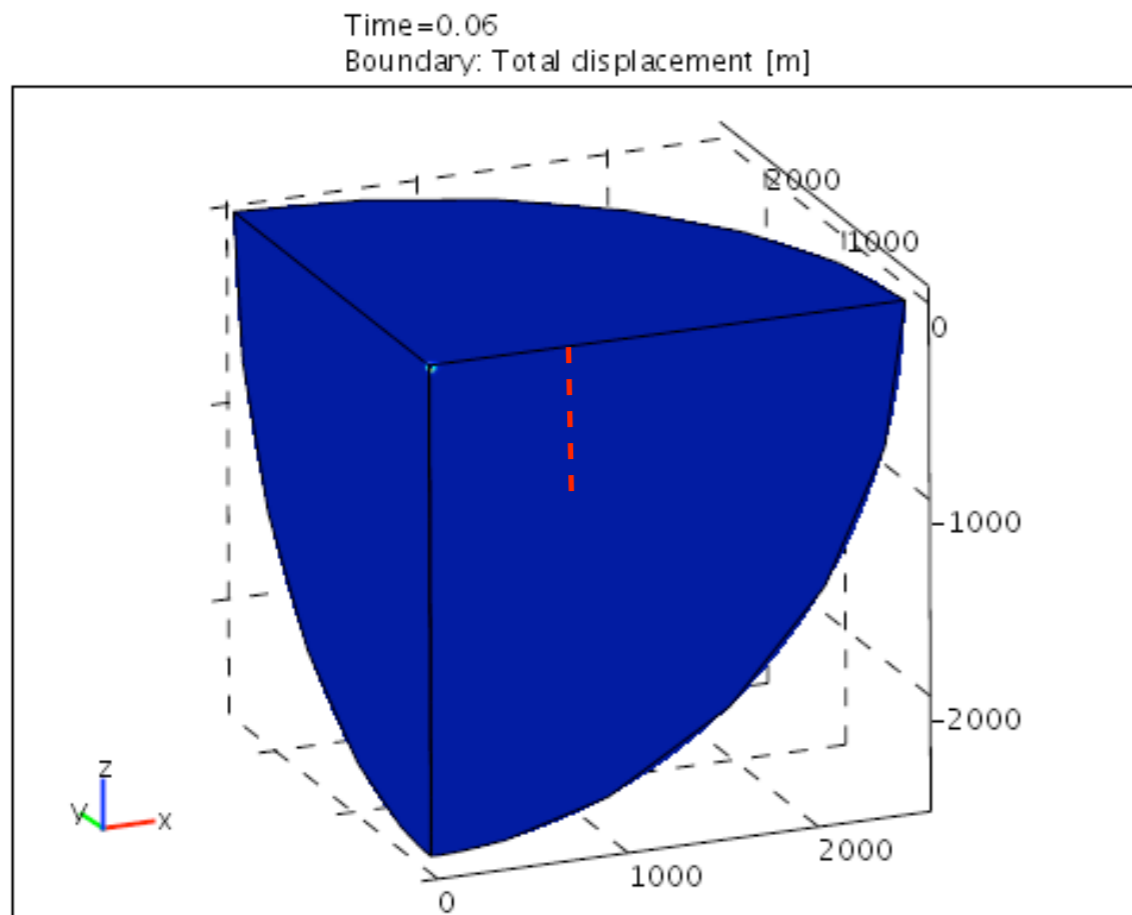
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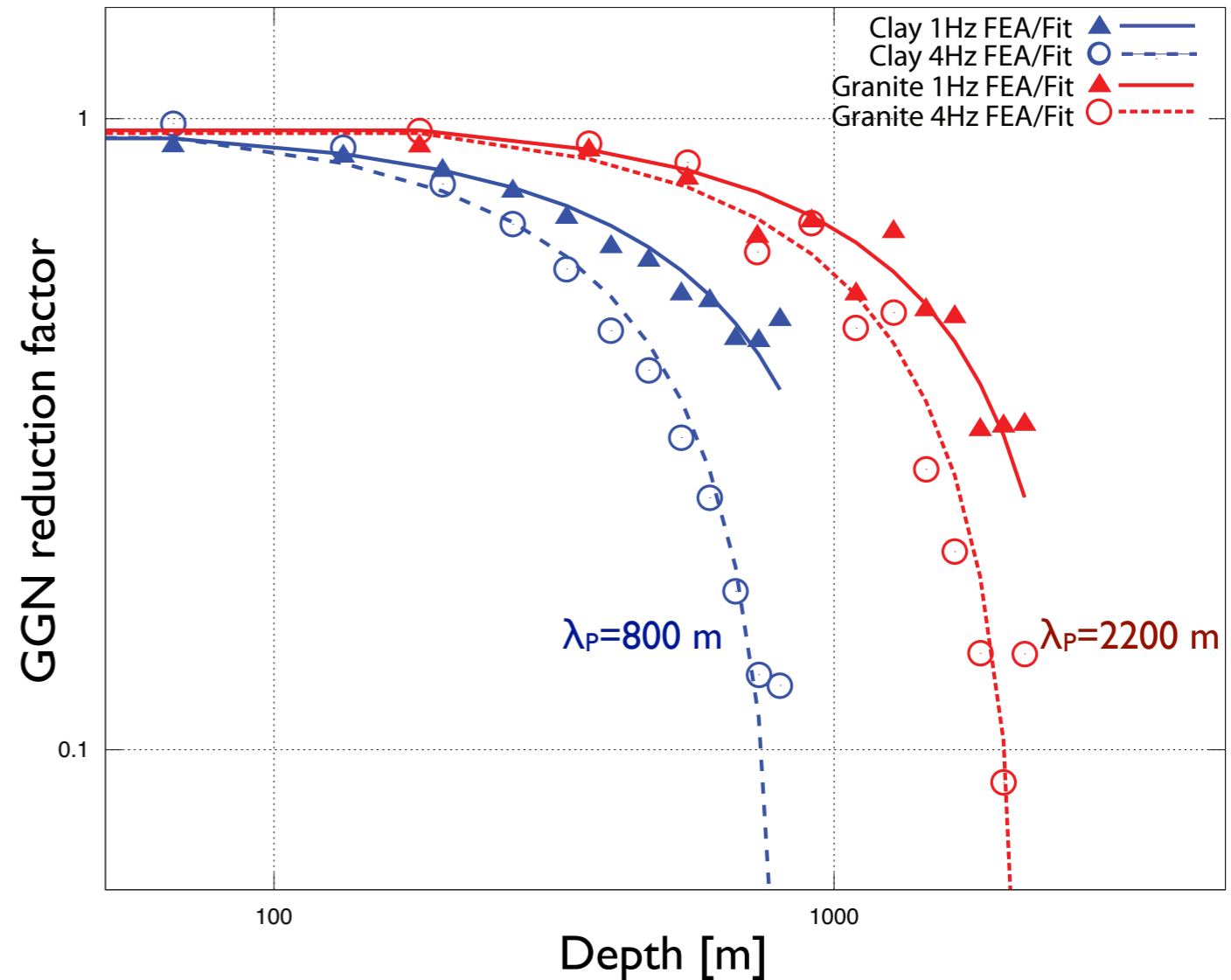
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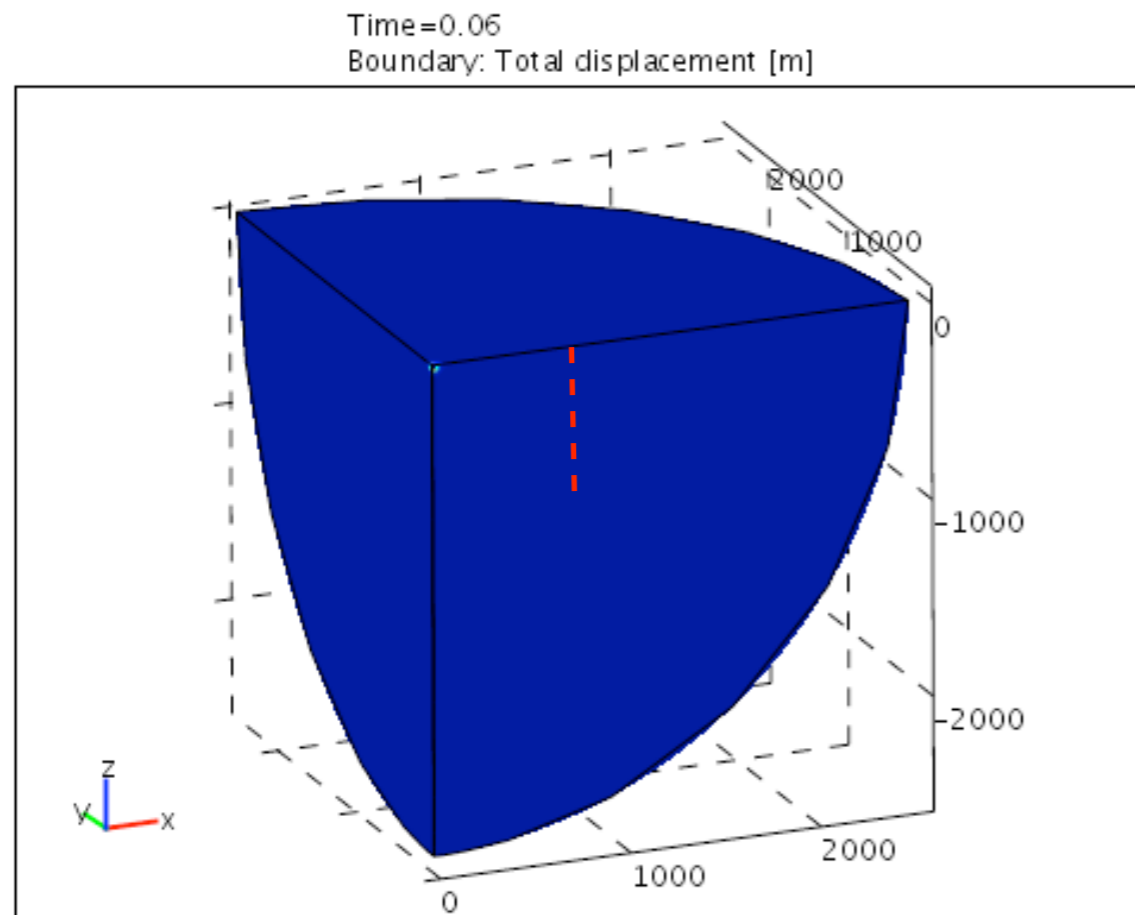
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GGN at depth / GGN at surface



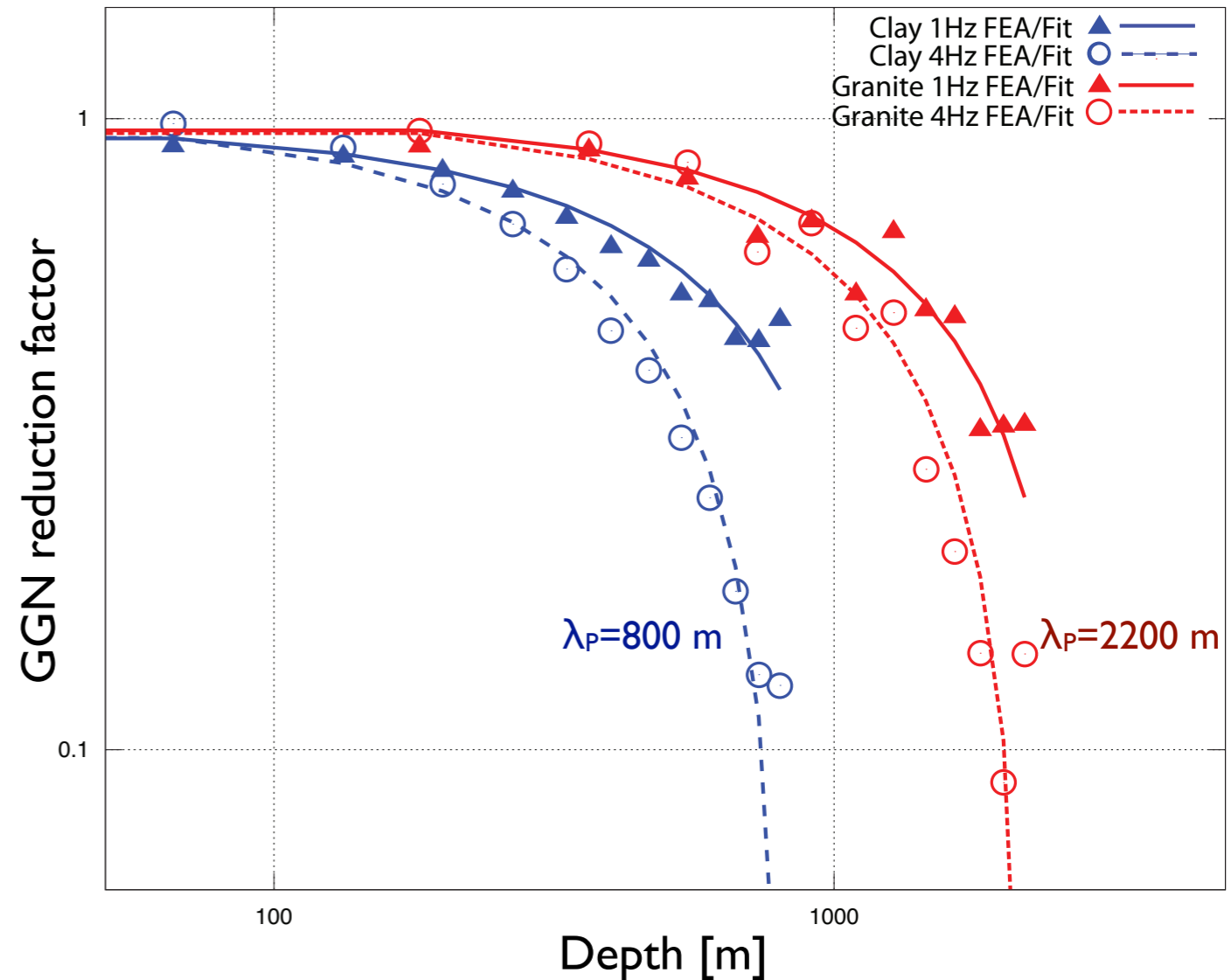
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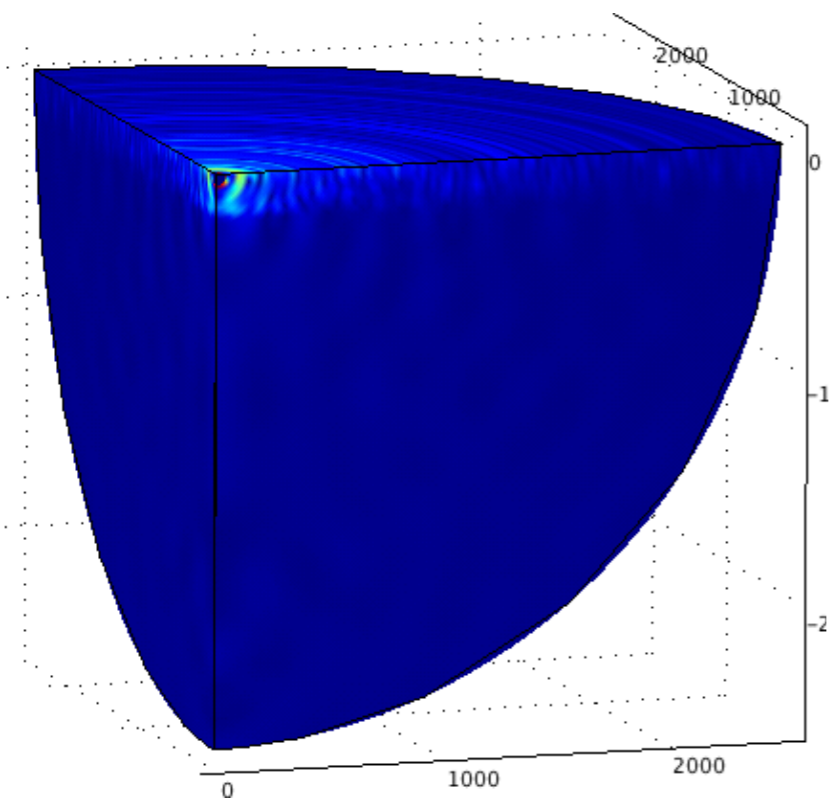
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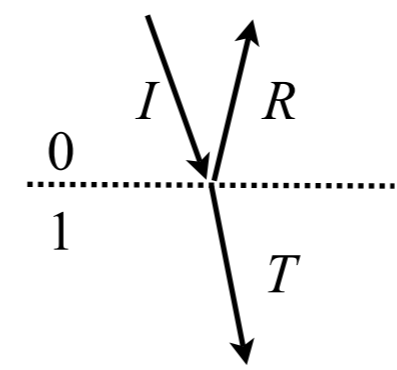


Clay and granite show similar properties when normalised to same force and λ_P

Multi layer geologies provide higher reductions factors by confining energy in top layers



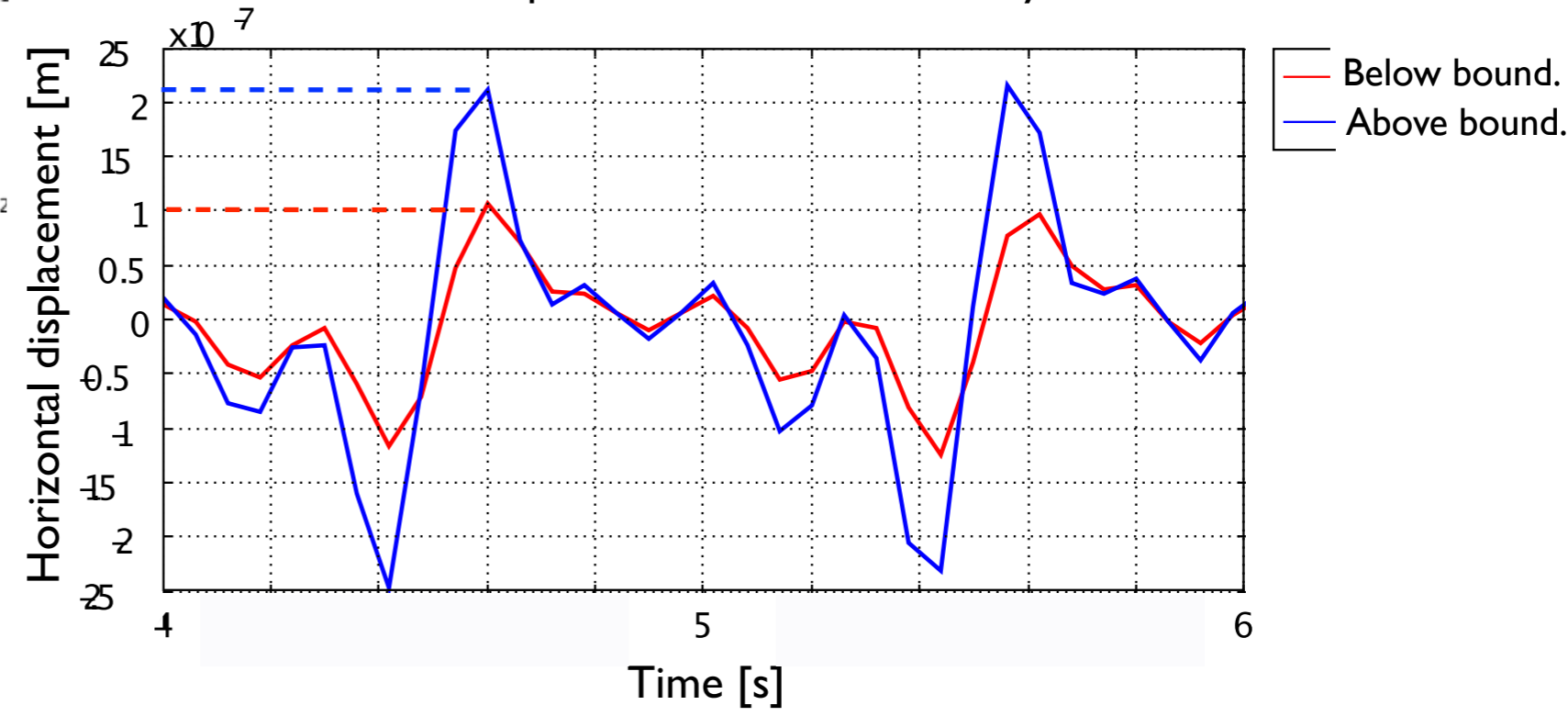
- Top layer: Clay 200 m thick
- Bottom layer: Granite



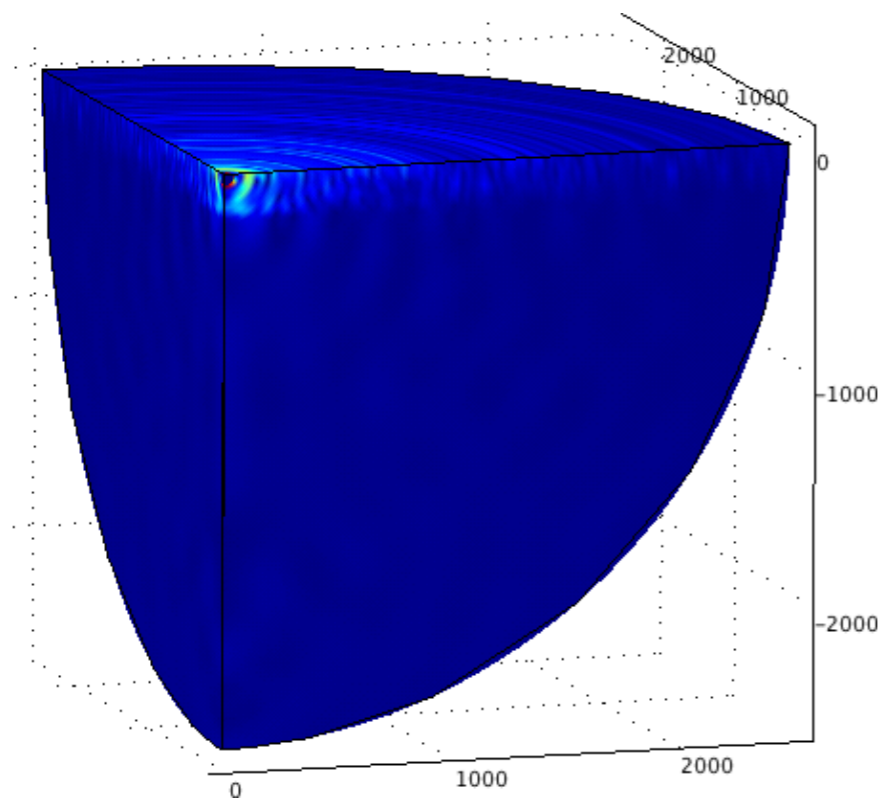
Horizontal shear wave transfer function

$$\frac{A_T}{A_I} = T_{SH} \approx \frac{2}{1 + \frac{c_1 \rho_1}{c_0 \rho_0}} \Big|_{\theta=0} = 0.45$$

Ground displacement across boundary

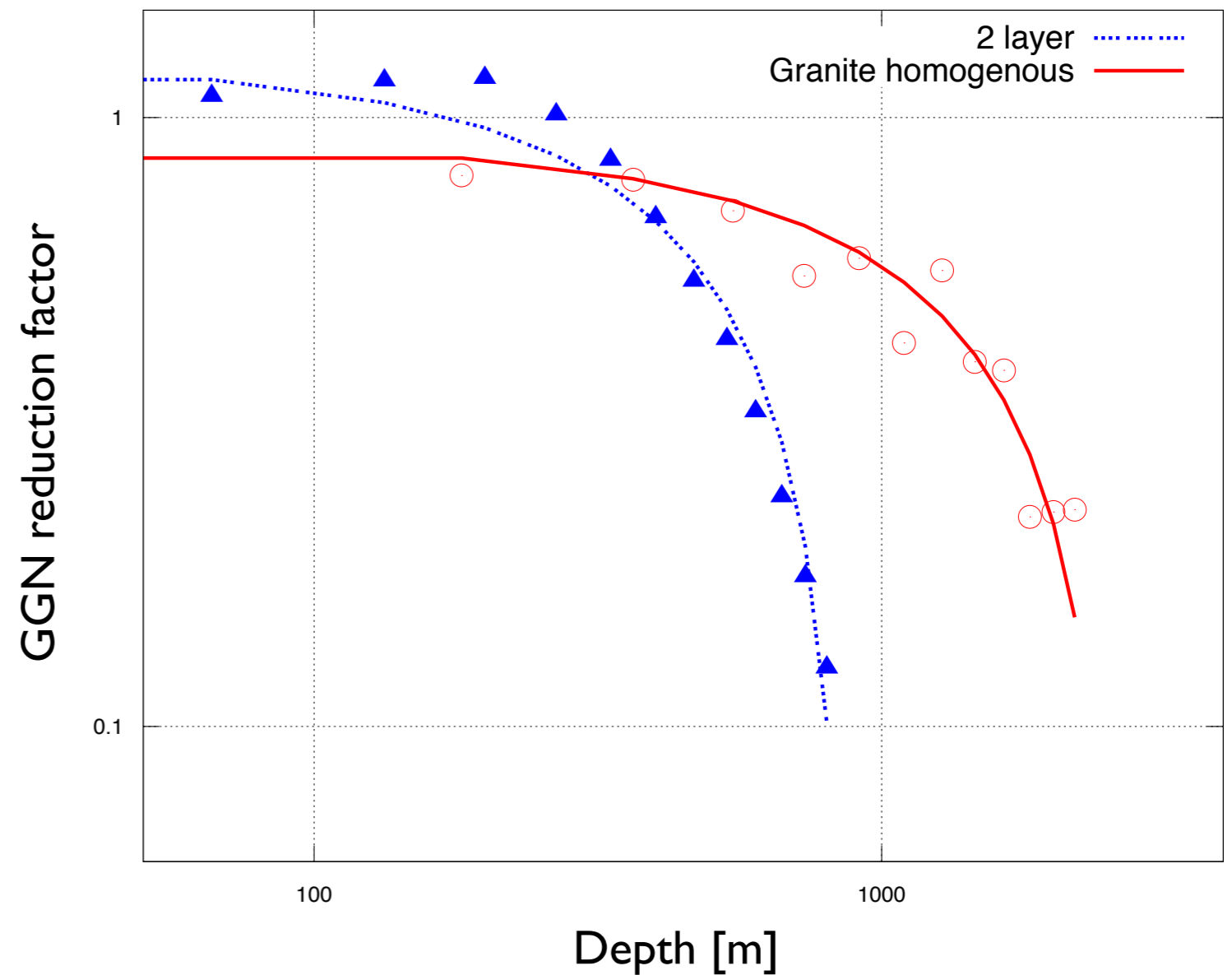


Double layer geologies provide higher reductions factors

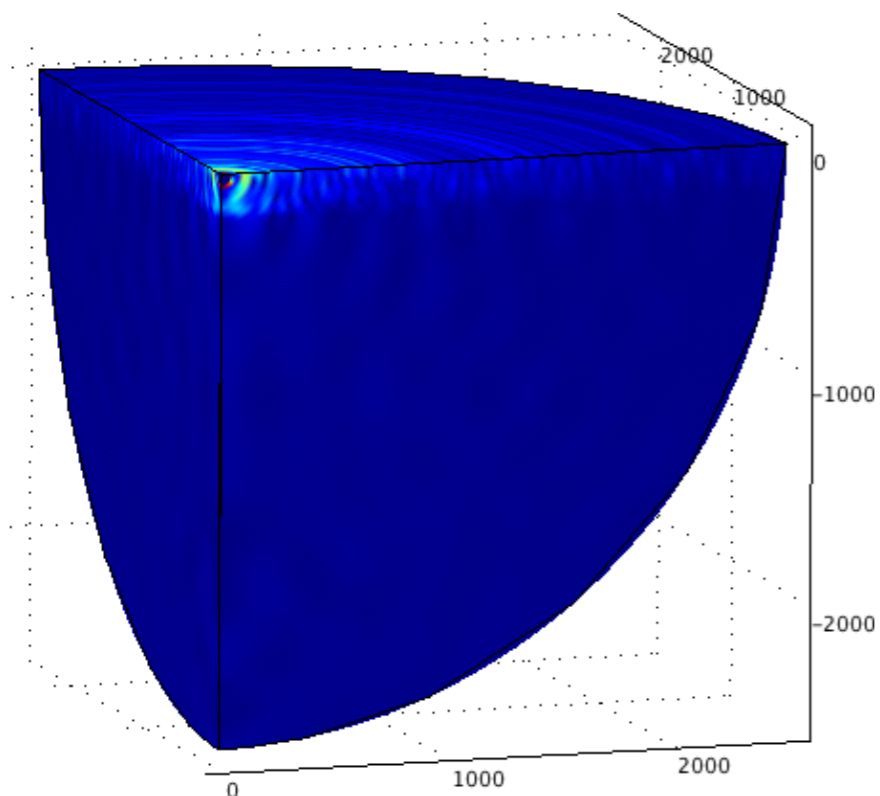


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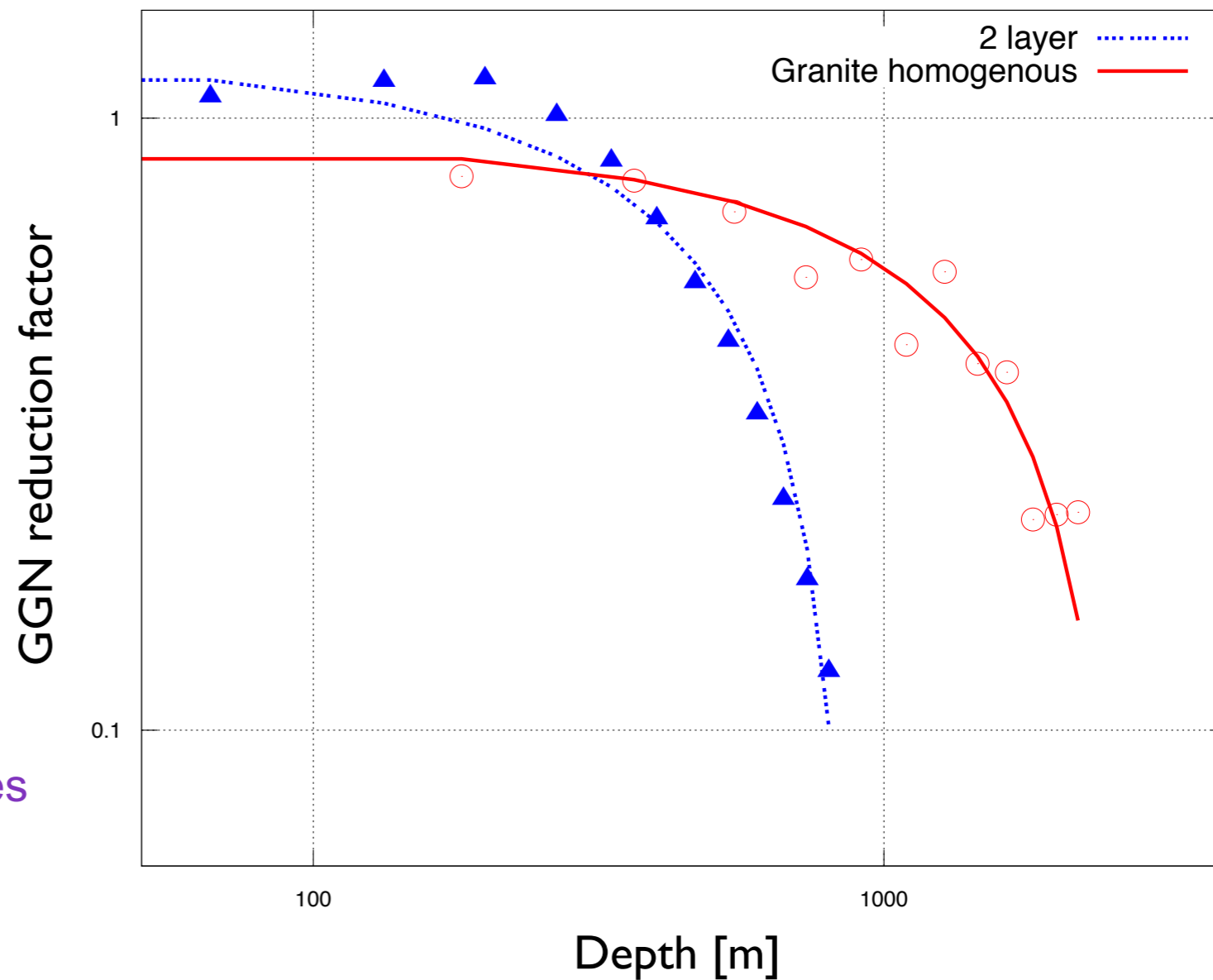


Double layer geologies provide higher reductions factors



- Top layer: Clay 200 m thick
- Bottom layer: Granite
- In this example reduction factor increases to ~10 without having to dig deeper
- Other ground properties possible to increase this even further

GGN at depth / GGN at surface



Ongoing research

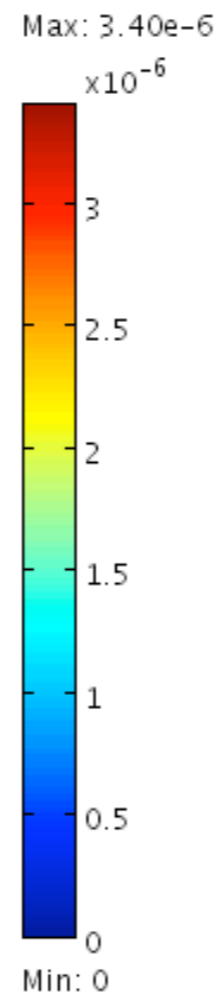
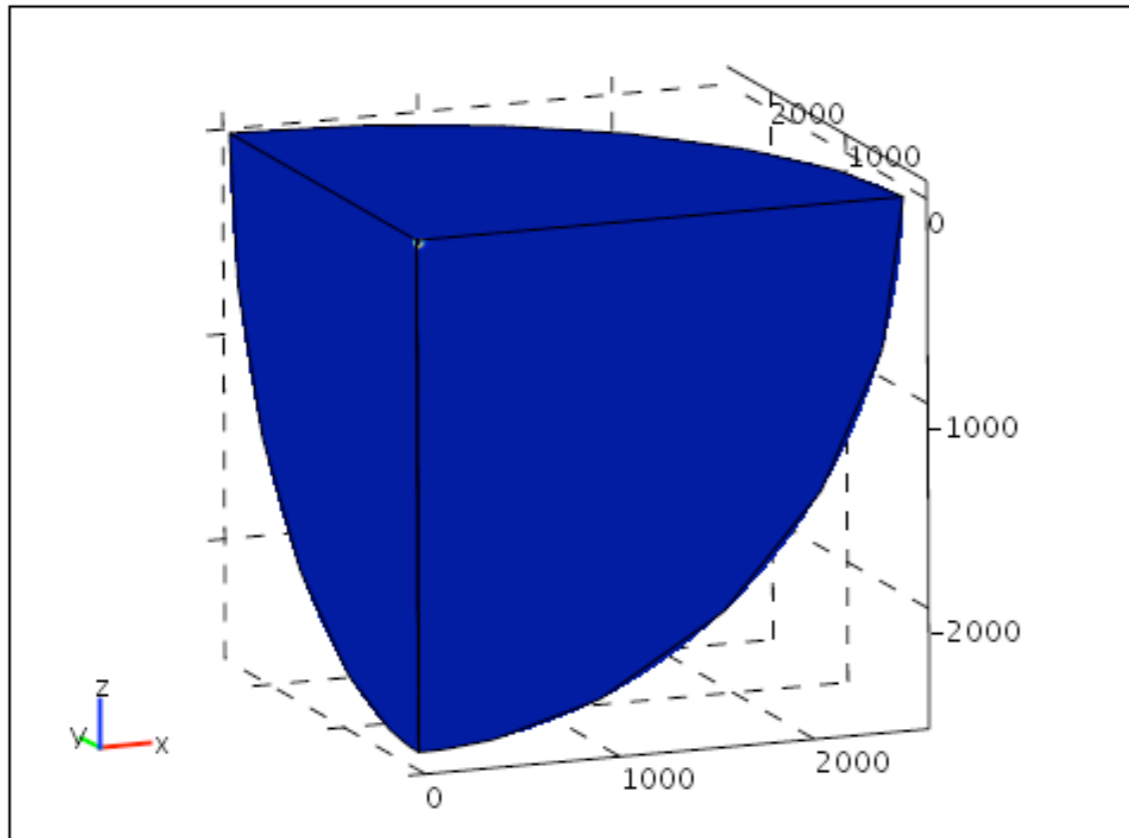


Homestake network - hard rock
Realmonite - salt
Future additional sites

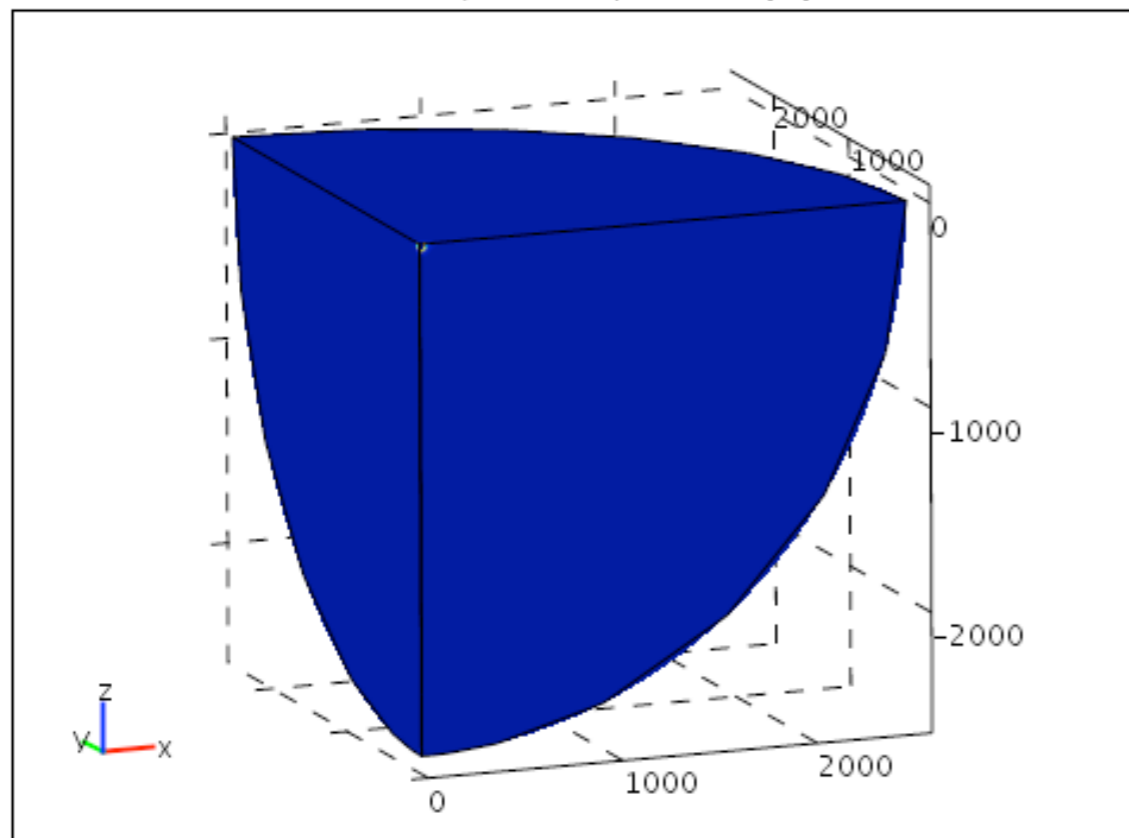
Conclusions

- ET requirements demand underground site
- FEA modeling of seismic wave fields
- Good agreement with analytical solutions
- Investigate
 - *Various geologies and excitations*
 - *GGN subtraction schemes*

Time=0.06
Boundary: Total displacement [m]

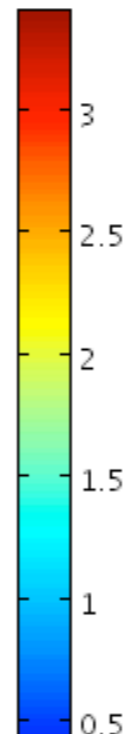


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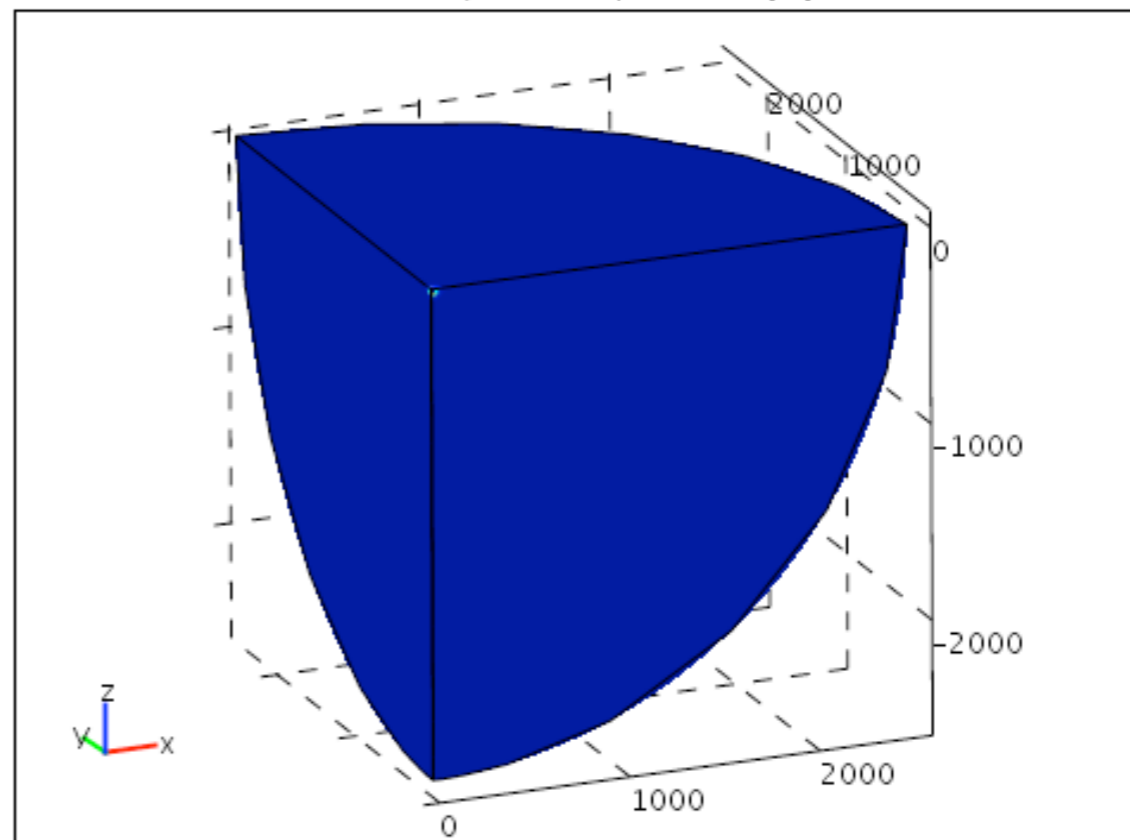


Max: 3.40e-6

x10⁻⁶

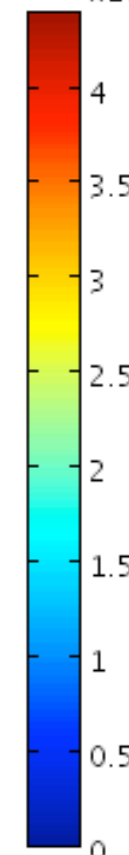


Time=0.06
Boundary: Total displacement [m]



Max: 4.39e-6

x10⁻⁶



Min: 0

Gravity gradient has a direct coupling to the ITF mirrors

- Seismic noise suppression
 - Development of superattenuators
- Gravity gradient noise
 - Cannot be shielded
 - Network of seismometers and development of data correction algorithms

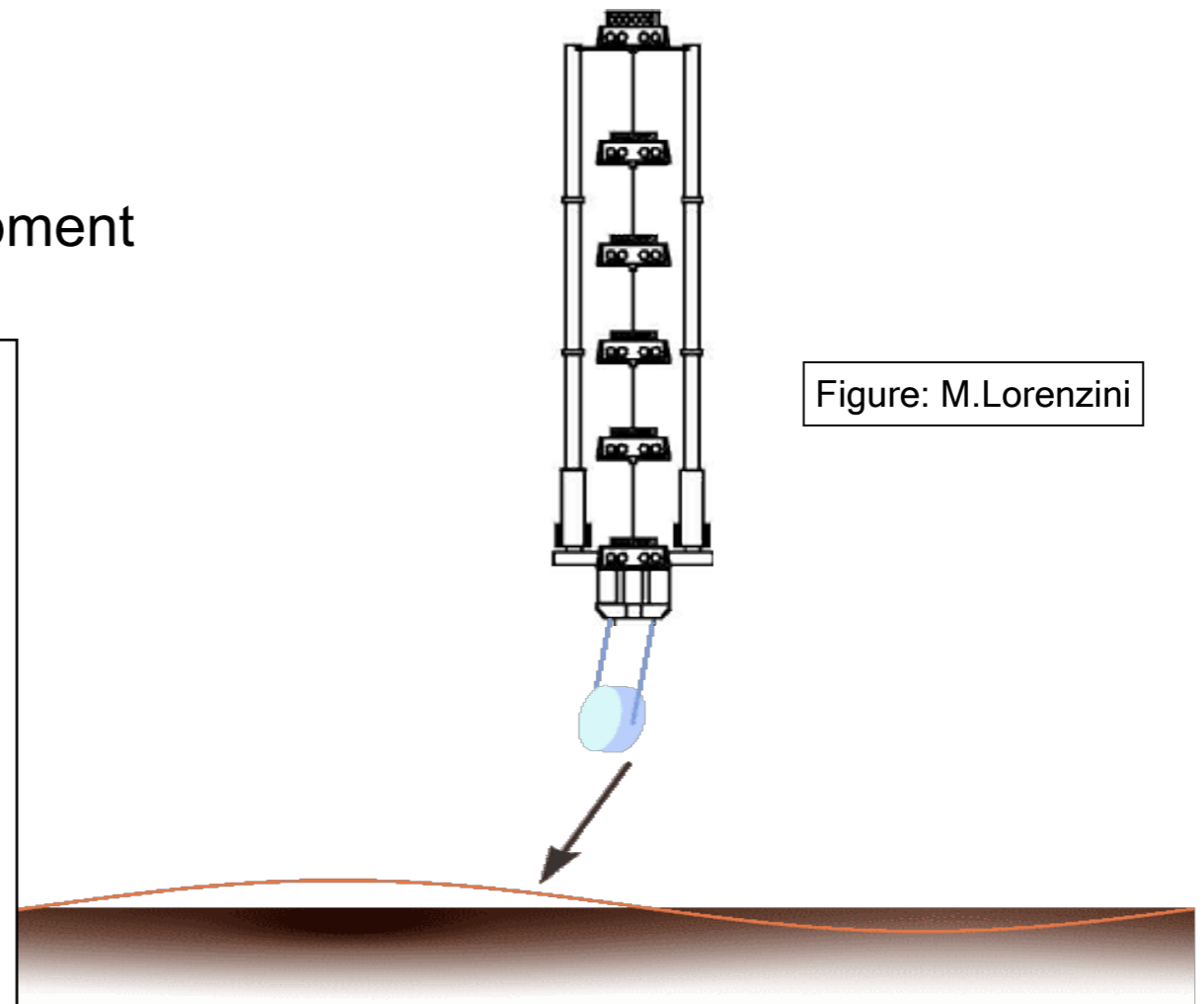
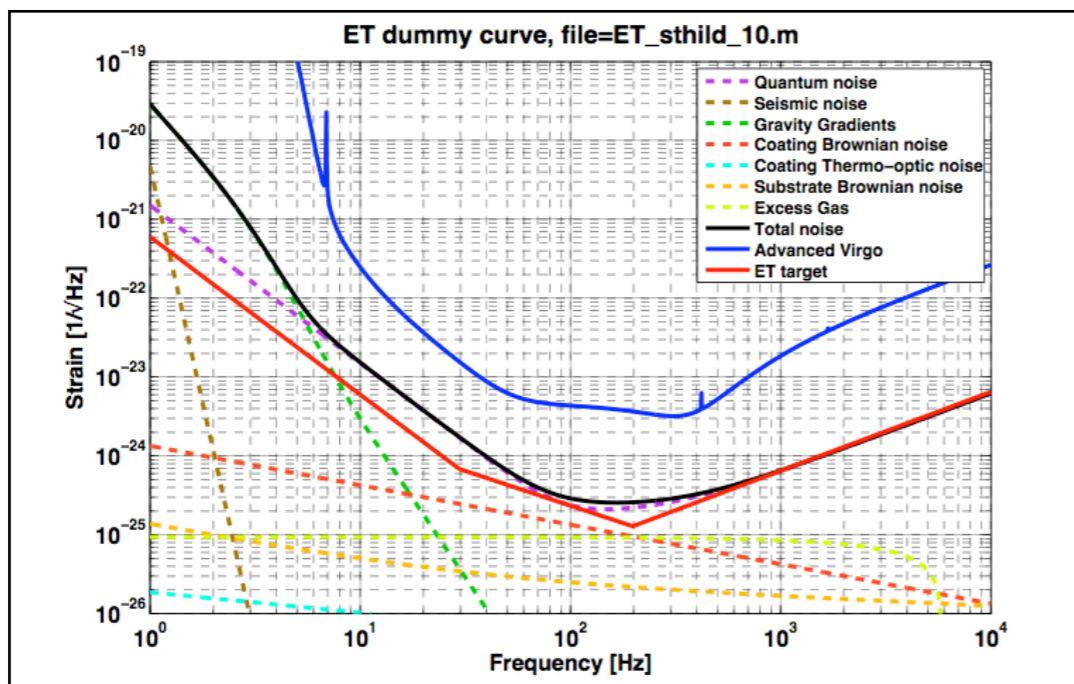
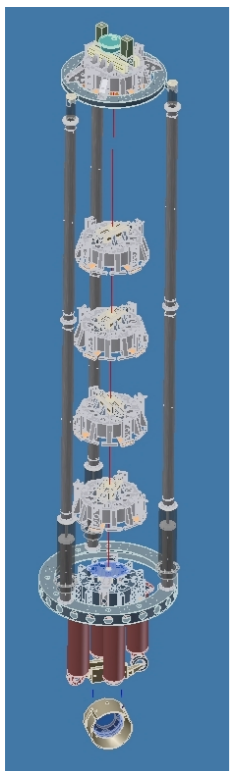
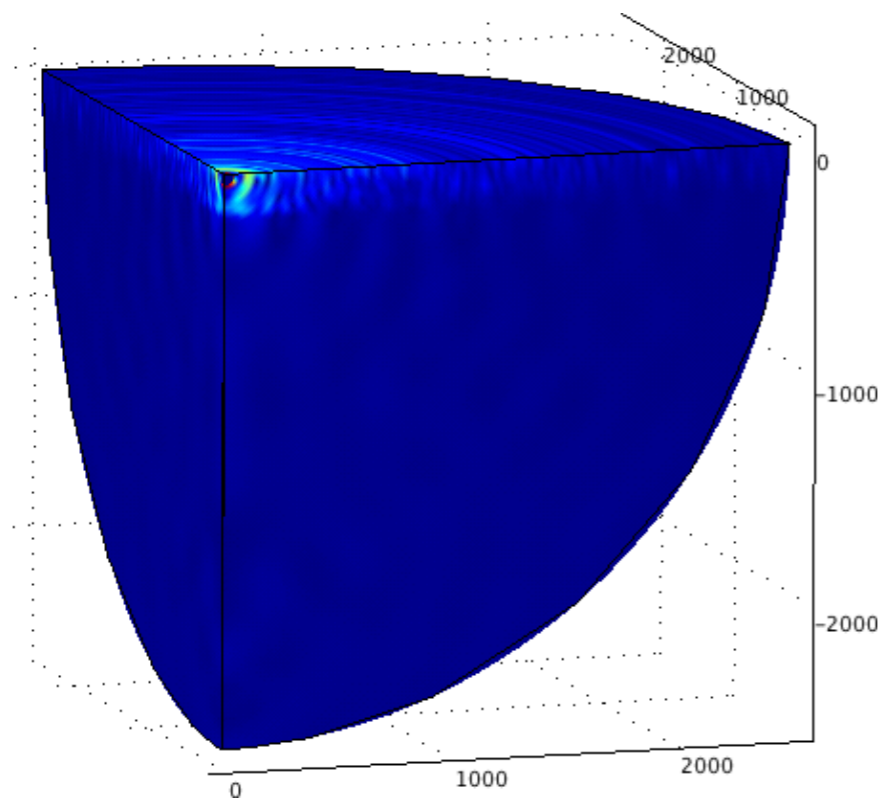


Figure: M.Lorenzini

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